

# Couplings



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# SKF Couplings

Flexible couplings are used to mechanically connect two shafts to transmit power from one shaft to the other. They are also able to compensate for angular, parallel or skew shaft misalignment in a torsionally rigid way. This is particularly important for applications where misalignment can affect the velocity and acceleration of the driven shaft. Coupling performance and reliability is directly affected by how it is installed, aligned and maintained.

To support the industry needs of increasing reliability and productivity whilst lowering cost, we combine an extensive application knowledge and experience, with the latest technology to develop tailored solutions. Whether your goal is to enhance equipment performance for increased customer value or to boost overall profitability, we have the couplings you need.

Our extensive range of standard and customised coupling products is available in various types, sizes, and capacity ratings to suit different applications and operating conditions. For large, heavy-duty applications, our couplings ensure optimum shaft contact, accommodating high torque values while reducing power loss and minimizing misalignment effects



# Coupling selection guide

### Introduction

There is an extensive range of couplings available on the market today. Unsurprisingly, selecting the best coupling for a particular application can be a complicated matter.

 A coupling can be simply defined as "a device that transmits power (torque) from one shaft to another, while allowing some degree of misalignment (angular, parallel or combined) between the two rotating shafts". In addition to the above definition, some couplings allow for axial (end-float) movement .

Also, couplings may be classified as either flexible or rigid.

Depending on its type, a coupling may be required to tolerate a variety of conditions during its service life.

Some of these functions could be to:

- Transmit power (torque)
- Permit and accommodate limited amounts of misalignment (angular and/or parallel)
- Allow for ease of assembly, maintenance and dis-assembly
- Allow for some amount of dampening (if required)
- Allow or compensate for end-float/axial movement/thermal expansion
- Retain rigidity between the connecting hubs and the shafts
- Withstand/compensate for temperature fluctuations/thermal growth
- Provide protection against overload of the driven machine
- Be of low inertia with minimal effects on the drive system
- Where necessary, provide good lubricant retention

For permanent couplings (couplings that are in-situ all the time, as opposed to clutches or non-permanent couplings), there are two main groups based on the transfer element, with typical features listed as follows:

Elastomeric couplings (transfer element typically a rubber or urethane compound or a derivative).

- Torsionally soft
- No lubrication required
- Generally less expensive (for similar torque capabilities) than metallic couplings
- Usually have field replaceable elements or elastomers
- Wide range of series available with some universal interchange

Metallic couplings (transfer element typically steel).

- Torsionally stiffer as compared to elastomeric couplings
- Offers best torque-to-diameter ratio with a higher power density
- Most competitive offer (for torque capacity)
- Excellent temperature range (usually limited by the oil seal material)
- Good chemical resistance
- Available in numerous materials (in some styles)
- Available with zero backlash

Considering the wide range of different coupling types and styles, many suitable solutions are possible.

Special note on engine (IC) drives Where the prime mover is an internal combustion (IC) engine, special consideration needs to be given to the number of cylinders, balance (flywheel), in conjunction with the driven machines' characteristics, especially in relation to the system's torsional vibration.

The type of coupling selected needs to be able to withstand, and compensate for, conditions not normally associated with electric motor or turbine prime mover systems.

#### Quick selection guide

In order to quickly assess which coupling offers the best solution based on application parameters, please refer to the basic pre-selection table on page 6.

These tables incorporate many factors that could determine (or eliminate) a coupling style by either operational or environmental considerations.

The service factors shown in this catalogue are based on the prime mover being an electric motor or turbine . Accordingly, the service factor must be increased for applications with IC engine prime movers.

### Selection parameters for SKF shaft couplings

The following table shows typical characteristics for various coupling types . To be used in determining which coupling type or style may be best suited for an application.

#### General notes:

The preceding table is a general comparison of the SKF range of couplings.

The values, where shown, are based on the best or highest value and may not represent the entire size range . Check the catalogue for details, especially if using different elastomer materials, as these can change not only temperature range and chemical resistance, but may also affect the torque capacity, and allowable misalignment, as often elastomers of varying durometer (Shore A° ) are used  $(\rightarrow$  note 4).

#### 1 Coupling type

E = Elastomer (with rubber (NBR) or urethane typically), or  $M =$  metallic (carbon steel typically)

#### 2 Maximum shaft capacity

- Based on metric shaft, with standard keyway dimensions to DIN 6885/1, or equivalent.
- Shallow keys can be used up to 150 mm only.

#### 3 Maximum torque

Values listed are for a service factor of 1 .00 . Refer to the relevant catalogues for recommended service factors. Note that they vary between coupling types.

#### 4 Maximum temperature

- The range covers standard design, unless stated otherwise . It should be noted that many of the elastomeric type couplings have a number of elastomer materials available to accommodate not only higher ambient/operating temperatures, but also higher torques (although with reduced alignment capability).
- For metallic-type couplings, it is important to note both the seal materials and the type of lubrication (usually grease) at both elevated and lower temperatures.

#### Selection parameters for shaft couplings



- Tyre for the SKF Flex Natural Rubber NR (Standard) –50 to +50 °C Chloroprene (FRAS) –15 to +70 °C (as shown in tables)
- Gear and grid: Normal operating temperature for standard seals is 120 $\degree$ C (intermittent<sup>1)</sup> up to 150 $\degree$ C). High temperature seals must be used above these temperatures. Maximum temperature for the higher temperature seals is 200 °C  $(260 °C$  intermittent<sup>1)</sup>).

#### 5 Chemical resistance

- Many elastomer-type couplings have different elastomer material options for chemical resistance . Note that the torque capability may be reduced!
- For SKF Flex, the "FR" chloroprene Tyre offers better chemical resistance, specifically to oils and greases, than standard natural rubber "NR" compound.
- Chemical resistance for gear and grid couplings is generally limited by the seal material (and any possible, though unlikely, reaction with the lubricant) .

• The ES-Flex coupling has 4 different elastomer sleeves available; Standard TPR (Thermo-Plastic Rubber); EPDM, Chloroprene and Hytrel.

#### 6 Adaptability in design

Refers to the ability and ease with which a coupling standard design can be adapted to vertical, spacer, floating shaft, brake types, along with options of either taper bushing, or QD.

#### 7 SKF designation

The ES-FLEX (elastomer-in-shear) is listed for the US market only.

8 Ease of installation for rigid couplings, while usually with few components, is considered poor, due to the necessity to have accurate alignment (often timeconsuming).

#### 9 Coupling capacity

For rigid couplings, the transmittable torque (MT) is usually determined by the shaft diameter rather than the coupling.



#### 10 Disc coupling misalignment

For the single configuration disc couplings, parallel offset is not permissible.

- When using double disc pack, i.e. with a spacer, the amount of parallel offset is proportional to the DBSE (Distance Between Shaft Ends) dimension.
- Generally there are values for permissible axial movement (δ) for disc couplings. As this movement can result in flexure fatigue, it can be critical in disc coupling selections.



 $\frac{1}{1}$  "Intermittent" is defined as a total of less than 1 000 hours of operation

# <span id="page-7-0"></span>Grid couplings

In high output (kW) and high torque applications where vibration, shock loads and misalignment occur, SKF Grid Couplings are an excellent choice.

The unique design of the grid and hub teeth enable these couplings to accommodate movement and stresses from all three planes, which can reduce vibration levels by as much as 30% .

The tapered grid element is manufactured from a high strength alloy steel. The grid, which, is the primary wear component of the coupling is designed for quick and easy replacement. Unlike other couplings, the hubs and other components are not disturbed. This makes realignment virtually unnecessary and further reduces

#### Grid couplings with taper bushing hub options

downtime and maintenance costs.

In addition to the standard plain bore hub that is offered with the grid couplings, there is the option to offer a taper bushing as a machined product.

In such circumstances there must be a re-rating of the coupling capacity, along with the reduction in the LTB hub width.

The taper bushing is normally mounted from the inner face of the coupling (Type F or flanged side configuration), but may, in certain sizes, be able to be mounted in the external ("H"or hub) configuration. However, as the hub diameter at the non-grid end is significantly reduced, a check on the location of the setscrews should be made, to avoid any stress fracture.

Page 18 may be used as a general guide as to what bushing fits the grid coupling hub, and by how much the LTB hub is reduced from the standard length  $(C)$ .

#### Gear and grid metallic couplings with braking capability

With regard to the SKF range of couplings, both the gear and the grid may be adapted for use in braking systems – typically disc or to a lesser extent nowadays, drum or shoe type brakes.

The selection of the coupling however, needs to be modified to allow for the peak loads encountered during braking (retardation).

Generally it will be the retarding torque imposed by the brake actuation that will determine the required coupling (subject to the maximum shaft capacity).

For brake-type grid couplings, the brake disc (or drum / shoe) would normally be mounted to the driveN (braked) machine. As the gear coupling is symmetrical, either hub can be the driveR or driveN.



*Horizontal split cover*



*Vertical split cover*



*Full spacer*



*Half spacer*

# Selection

## Standard selection method

This selection procedure can be used for most motor, turbine, or engine driven applications . The following information is required to select an SKF grid coupling:

- Torque power [kW]
- Speed [r/min]
- Type of equipment and application
- Shaft diameters
- Shaft gaps
- Physical space limitation
- Special bore or finish information

Exceptions to use of the standard selection method are for high peak loads and brake applications . For these, use the formula selection method or contact SKF.

1 Determine system torque If torque is not given, use the following formula to calculate for torque (T)

Power [kW] × 9 550 System torque = –––––––––––––––––– Speed [r/min]

#### 2 Service factor

Determine the service factor from tables 9 to 10 on pages 87 to 88.

#### 3 Coupling rating

Determine the required minimum coupling rating as shown below:

Coupling rating = service factor × torque [Nm]

#### 4 Size

Select the appropriate coupling from the torque column of the product tables on pages 16 to 20 with a value that is equal to or greater than that determined in step 3 above and check that the chosen coupling can accommodate both driving and driven shafts.

#### 5 Other considerations

Possible other restrictions might be speed [r/min], bore, gap and dimensions .

### Standard selection example

Select a coupling to connect a 30 kW, 1 440 r/min electric motor that is driving a boiler feed pump. The motor shaft diameter is 55 mm, pump shaft diameter is 45 mm . Shaft extensions are 140 mm and 110 mm. The coupling to be selected will replace a gear type coupling with a 3 mm gap.

1 Determine system torque System torque [Nm] =

 $\frac{30 \text{ kW} \times 9550}{1440 \text{ r/min}}$  = 199 Nm

2 Service factor From table 9 on page  $87 = 1.50$ 

#### 3 Required coupling rating

 $1.5 \times 199$  Nm = 298.5 Nm

4 Size

From product tables on page 16, the coupling size 1060 is the proper selection based on the torque rating of 684 Nm which exceeds the required minimum rating of 298.5 Nm as well as accommodating driving and driven shaft diameter requirements.

#### 5 Other considerations

The speed capacity of 4 500 (coupling size 1060) exceeds the required speed of 1440 r/min. The maximum bore capacity of 57 mm exceeds the required shaft diameters of 55 mm and 45 mm . The resulting service factor is 2.29. This will provide a very good service life for the coupling and a high level of reliability.

## Formula method

The standard selection method can be used for most coupling selections . However, the formula method, should be used for:

- high peak loads
- brake applications (if a brake wheel is to be an integral part of the coupling)

By including the system's peak torque, frequency, duty cycle and brake torque ratings, a more accurate result will be obtained.

1 High peak loads Use one of the following formulas

(A, B, or C) for:

- Motors with higher than normal torque characteristics .
- Applications with intermittent operations resulting in shock loads.
- Inertia effects due to frequent stops and starts or repetitive high peak torques.

Peak torque is the maximum torque that can exist in the system. Select a coupling with a torque rating equal to or exceeding the selection torque values obtained from the formulas below .

#### A Non-reversing peak torque selection

Torque [Nm] = system peak torque

or

Selection torque [Nm] =

 System peak kW × 9 550 –––––––––––––––––––––– r/min

#### B Reversing high peak torque Selection torque [Nm] =

 2 × system peak torque –––––––––––––––––––– r/min

#### C Occasional peak torques (non-reversing)

If a system peak torque occurs less than 1 000 times during the expected coupling life, use the following formula:

Selection torque [Nm] =  $0.5 \times$  system peak torque

or

Selection torque [Nm] =

 0 .5 × system peak kW × 9 550 –––––––––––––––––––––––––– r/min

#### 2 Brake applications

If the torque rating of the brake exceeds the motor torque, use the brake rating as follows: Selection Torque [Nm] = Brake torque rating x service factor.

## Formula selection example

#### High peak load

Select a coupling for reversing service to connect a gear drive low speed shaft to a metal forming mill drive . The electric motor rating is 30 kW and the system peak torque at the coupling is estimated to be 9 000 Nm. Coupling speed is 66 r/ min at the gear drive output with a shaft gap (between ends) of 180 mm .

#### 1 Type

Refer to product tables on pages 16 to 20 and select the appropriate coupling type.

2 Required minimum coupling rating Use the reversing high peak torque formula in step 1B.

 $2 \times 9000$  Nm = 18000 Nm = Selection torque

#### 3 Size

From product table on page 16, size 1130 with a torque rating of 19 900 which exceeds the selection torque of 18 000 Nm.

#### 4 Other considerations

Grid coupling size 1130 has a maximum "DBSE" dimension (distance between shaft ends) of 205 mm; the shaft hub has a maximum bore of 190 mm .

Note: See product table on page 16. The T hub has a maximum bore of 170 mm and the allowable speed of 1 800 r/min .

#### Formula method for brake disc applications

To determine the capacity required for a dynamic brake application:

$$
(1a) M_{TB} = \frac{kW \times 60 \times 10^3}{2 \times \pi \text{ r/min}} = x 2.0 \text{ [Nm]}
$$

which may be simplified to:

$$
(1b) M_{TB} = \frac{kW \times 9550}{r/min} = x 2.0 \text{ [Nm]}
$$

Additionally, where the inertias involved (I) are known or can be determined (by reference to the brake position), and the braking deceleration time, in rads/sec  $(\alpha)$  is known, the torque may also be determined from:

(1c)  $M_{TR} = 1 \times \alpha \times 2.0$  [Nm]

The coupling capacity [MT] from the catalogue must be greater than the figures obtained in 1(a), 1(b) or 1(c) above.

 $(2)$  M<sub>TNOM</sub>  $\geq$  MTB [Nm]

Note: Where the brake is only being used as a holding brake, i.e. the system is brought to a stop by other means, prior to application of the brake, standard coupling selection procedures may be used.

(a) Grid coupling with brake disc (schematic only)  $(\rightarrow$  fig. 1).

The grid coupling usually consists of the following SKF components:

A major advantage of using the gridtype coupling (TGH) is that the covers are horizontally split, thus allowing ease of access to the grid for replacement. No additional axial spacing is required – something that can be critical, as brake calipers and actuator mechanisms can take up space.

#### Note:

#### a. Brake disc dimensioning

- In general the coupling selection for dynamic braking should be no less than 200% of the running (installation) torque, unless the results of a full analysis of the inertias involved are known, along with the desired stopping time.
- The diameter of the brake disc (Db), will be determined from the required torque, and the caliper's force at the effective diameter (Dcal in the above diagrams) at which the caliper unit (or units) will engage.
- Multiple calipers, typically no more than two, are generally set 180° apart. The thickness of the disc, and whether plain or ventilated, will also be determined by
	- *–* the inertias ∑ I (kgm<sup>2</sup>) being retarded, relative to the brake position,
	- the stopping time t<sub>s</sub> (in seconds) required

#### b. Brake disc (general)

- International standards, such as DIN 15435, have tables of recommended diameters and thicknesses (or widths) for both disc and drum (shoe) type brakes . (Many brake-system manufacturers also have their own factory standards).
- Disc material will vary depending on the application, capacity and the amount of energy that is required to be dissipated during engagement. Typically however, they are made of spheroidal graphite (nodular) cast iron (e .g . DIN GGG40, AISI 60-40-18; JIS FCD400).
- Thickness variation overall should be <0 .05 mm total, and surface finish  $≤0.002$  μm.



# Engineering data

For additional useful information on grid couplings, such as an interchange guide, misalignment capability, puller bolt hole, inertia and standard stock spacer lengths data, please refer to tables 1 to 7.

## Order data

A complete grid coupling consists of 2 hubs, a cover and a grid. For further details and options refer to table 8, pages 12 and 13.





#### SKF grid coupling interchange guide

Vertical split cover



#### Table 4

<span id="page-11-0"></span>Puller bolt hole data (grid)



 $B.C.D.<sup>1</sup>$  Bolt size

PHE 1110TGRSB 149  $\frac{1}{2}$ <br>PHE 1120TGRSB 168  $\frac{1}{2}$ <br>PHE 1130TGRSB 197 5/<sub>8</sub>

**PHE 1150TGRSB** 263  $\frac{3/4}{4}$ <br>**PHE 1160TGRSB** 298  $\frac{3/4}{4}$ PHE 1170TGRSB 338 1"-8 PHE 1180TGRSB 378 1"-8 PHE 1170TGRSB 338 1"-8<br>
PHE 1180TGRSB 378 1"-8<br>
PHE 1190TGRSB 413 1"-8

PHE 1200TGRSB 456 1"-8<br>
PHE 1210TGRSB 497 11/2<br>
PHE 1220TGRSB 541 11/3 PHE 1210TGRSB  $1^{1/2}$ <br>PHE 1220TGRSB 541  $1^{1/2}$ 

PHE1230TGRSB 586 1 $\frac{11}{2}$ <br>PHE1240TGRSB 633 1 $\frac{1}{2}$ <br>PHE1250TGRSB 690 1 $\frac{1}{2}$ 

PHE 1100TGRSB 133

PHE 1140TGRSB 236<br>
PHE 1150TGRSB 263<br>
PHE 1160TGRSB 298

– mm Tr (UNC)

 $3/8 - 16$ 

"-13 "-13 "-11

"-10 "-10 "-10

"-6 "-6

"-6<br>"-6<br>"-6

 $1\frac{1}{2}$  -6



Misalignment capability







 $1)$  B.C.D. = Bolt Centre Diameter

PHE1260TGRSB 749



<sup>1)</sup> For bored-to-size designations, add bore size. For example, PHE 1050TG25MM<br>The cover assembly kit is supplied with the cover. The spacer hub assembly kit is supplied with the spacer hub set.<br>The assembly kit is suppli

### Table 6

Table 7

#### Full spacer coupling

TGFS Standard stock spacer lengths (DBSE = Distance between shaft ends)





The values are based on hubs with no bore.



# <span id="page-13-0"></span>Installation

The performance of the coupling depends largely upon how it is installed, aligned and maintained .

SKF Grid Couplings are designed to operate in either a horizontal or a vertical position without modification.

1 Mount the seals and the hubs Clean all metal parts using non-flammable solvent and check hubs, shafts and keyways for burrs and remove if necessary . Lightly coat the seals with grease and place well back on the shafts before mounting the hubs. Mount the hubs on their respective shafts so that each hub face is flush with the end of the shafts  $(\rightarrow$  fig. 1).

#### 2 Gap and angular alignment

Using a feeler gauge equal in thickness to the gap specified in table 5 on page 12 . Insert the gauge as shown in image  $(\rightarrow$  fig. 2) to the same depth at 90° intervals and measure the clearance between the gauge and hub face. The difference in the minimum and the maximum measurements must not exceed the angular limits specified in table 5 on page 12.

#### 3 Offset alignment

Align the two hubs so that a straight edge rests squarely on both hubs and also at 90° intervals (Fig. 3). The clearance must not exceed the parallel offset installation limits specified in table 5 on page 12 . Tighten all foundation bolts and repeat steps 2 and 3. Realign the application if necessary.

#### 4 Mount the grid

Pack the gap and all of the grooves in the two hubs with a specified lubricant (**†** page 94) before mounting the grid . Fit the grid over the hubs by starting at one cut end, work the coils of the grid tooth by tooth in one direction and seat firmly as you go with a soft mallet  $(\rightarrow$  fig. 4).

#### 5 Pack with grease and assemble the covers

Pack the spaces between and around the grid with as much lubricant as possible and wipe off the excess so that it is flush with the top of the grid (→ fig. 5). Position the seals on hubs so they line up with the grooves in the cover . Position gaskets on the flanges of the lower cover half and assemble the covers so that the match marks are on the same side . Push gaskets in until they stop against the seals and secure cover halves with the fasteners provided and tighten them accordingly. Make sure that the gaskets stay in position during this tightening procedure ( $\rightarrow$  fig. 7). Once the coupling is completely assembled, remove both of the lubrication plugs in the cover and insert a lubrication fitting. Then, pump in the appropriate lubricant until it is forced out of the opposite lubrication hole ( $\rightarrow$  fig. 8). Replace the two lubrication plugs and the installation is complete.

## Grid removal

Whenever it is necessary to replace the grid, first remove the cover halves and set aside. Beginning at the cut end of the grid, carefully insert a screwdriver into the loop  $(\rightarrow$  fig. 9). Using the hub teeth for leverage, gradually pry the grid up, alternating sides while working around the coupling.

SKF does not recommend re-using the removed grid.























Cover profiles



Sizes 1020–1140





Sizes 1150–1200

Sizes 1210–1260



Horizontal split cover couplings are high performance, general purpose and easy to maintain .

The grid is designed to be replaced without disturbing any other component in the drive.<br><sup>1)</sup> Contact SKF for bore dimensions of these coupling sizes





Vertical split cover couplings are high performance, general purpose and easy to maintain .

The grid is designed to be replaced without disturbing any other component in the drive . The vertical cover allows for higher running speeds .







 $^{11}$  Bore capacities are based on standard ISO keyway dimensions to ISO773 (DIN6885/1) unless otherwise stated. For full coupling dimensions and technical details, refer to **page 12.**<br>2) The limitations in the couplings





SKF horizontal split cover full spacer couplings are designed to accommodate long distances between the shafts that are to be connected.<br>This coupling gives you the added advantage of being able to drop out the entire cent





SKF horizontal split cover half spacer couplings are designed to be used where there is no need to accommodate long distances between the shafts. It provides an economical alternative to<br>the full spacer and is an ideal cho

# Gear couplings

Very high-torque ratings, along with unparalleled bore capacities, give this coupling a great advantage over other types of couplings . SKF Gear Couplings are rated up to 1 310 kNm with a maximum bore of 525 mm . This is a heavy duty coupling with incredible design flexibility, making it an economical choice for many applications.

The unique design of the gear couplings tooth crowning dramatically reduces backlash and radial clearance . The hub bore capacities are the largest in the industry, allowing for low cost and long service life .

In some applications it is not possible to go up in coupling size to accommodate a specific torque requirement, usually due to dimensional restraints or operating speeds.

For coupling sizes over size 80GC, there are two options for increasing the torque capacity of the SKF Gear Coupling.

- 1 Heat treatment of the standard carbon steel hubs and cover sets (Type HT). (Note: This CANNOT be done retrospectively).
- 2 The use of alloy steel, heat-treated, to improve capacity by between 35–40% (Type XP) .

The correct selection and use of the relevant service factors however, is critical in these series, and should be referred to SKF PTP for full application analysis.

Conversely, higher speeds may also be obtained if the units are dynamically balanced. This should be mandatory over the standard speeds indicated in the tables.





*Double engagement* **†** *page 30*



*Single engagement † page 31*



*Double engagement † page 30 Double engagement spacer † page 33*



*Vertical double engagement † page 34 Rigid flanged sleeve † page 37*



*Slide single and double engagement* **†** *pages 35 and 36*





*Floating and vertical shaft single engagement † pages 41 and 43*

#### Gear couplings with taper bushing hub options

In addition to the standard plain bore hub offered with the gear couplings, there is the option of a taper bushing as a machined product.

In such circumstances there must be a re-rating of the coupling capacity, along with possible reduction in the LTB hub width. The capacity limitations are based on the maximum recommended torque for the relevant bushing, with a standard keyway.

The taper bushing is normally mounted from the inner face of the coupling (Type F configuration), sometimes referred to as inboard side). It may also be possible for it to be mounted in the external (H) configuration (or outboard). As the flex halves for the agma compliant couplings may also be interchanged, a combination of 'F' and 'H' hub can also be used where mounting conditions permit (e.g. FF, HH or FH / HF combinations).

The following table may be used as a general guide . It shows which bushing fits where, and defines any required reduction of the LTB hub from the standard (catalogue) length.

Note: As gear couplings traditionally offer the highest torque capacity vs . diameter ratio of any coupling, the range available with a taper bushing hub is limited. It becomes uneconomical to use this system when the derating of the coupling (due to the taper bushing limitation) falls well below the capability of the coupling with standard shaft connections.

# Selection

### Standard selection method

This selection procedure can be used for most motor, turbine, or engine driven applications . The following information is required to select an SKF gear coupling:

- Torque Power [kW]
- Speed [r/min]
- Type of equipment and application
- Shaft diameters
- Shaft gaps
- Physical space limitation
- Special bore or finish information

Exceptions to use of the standard selection method are for high peak loads and brake

applications . For these, use the formula selection method or contact SKF.

#### 3 Determine system torque

If torque is not given, use the following formula to calculate for torque (T)

System torque [Nm]=

Power [kW] × 9 550 Speed [r/min]

4 Service factor Determine the service factor with tables 9 and 10 on pages 87 and 88.

5 Coupling rating Determine the required minimum coupling rating as shown below:

Coupling rating = service factor × torque [Nm]

6 Size

Select the appropriate coupling from the torque column of the product tables on pages 30 to 38 and 41 to 44. with a value that is equal to or greater than that determined in step 3 above and check that the chosen coupling can accommodate both driving and driven shafts.

#### 7 Other considerations

Possible other restrictions might be speed [r/min], bore, gap and dimensions .

## Standard selection example

Select a coupling to connect the low speed shaft of an ore conveyor drive to a speed

reducer. The 350 kW, 1440 r/min electric motor is driving the reducer with an output speed of 38 r/min. The reducer low speed shaft diameter is 215 mm, the conveyor head shaft is 225 mm. Shaft extensions are both 280 mm.

1 Determine system torque System torque [Nm] =

> 350 kW × 9 550  $= 87997$  Nm 38 r/min

2 Service factor From table 7 on page  $85 = 1.00$  3 Required coupling rating  $1.00 \times 87951$  Nm = 87951 Nm

#### 4 Size

From product table on page 30, the coupling size 60 is the proper selection based on the torque rating of 90 400 Nm which exceeds the required minimum rating of 87 951 Nm.

#### 5 Other considerations

The speed capacity of 2 450 (coupling size 60) exceeds the required speed of 38 r/min . The maximum bore capacity of 244 mm exceeds the required shaft diameters of 215 mm and 225 mm . The minimum required shaft length (J) of 169 mm is exceeded by the equipment's shaft extensions of 280 mm . The resulting service factor is 1.03.

## Formula method

The standard selection method can be used for most coupling selections . However, the formula method should be used for:

- high peak loads
- brake applications (If a brake wheel is to be an integral part of the coupling)

By including the system's peak torque, frequency, duty cycle and brake torque ratings, a more accurate result will be obtained.

1 High peak loads

Use one of the following formulas (A, B, or C) for:

- *–* Motors with higher than normal torque characteristics.
- *–* Applications with intermittent operations shock loading.
- *–* Inertia effects due to frequent stops and starts or repetitive high peak torques.

Peak torque is the maximum torque that can exist in the system. Select a coupling with a torque rating equal to or exceeding the selection torque from the relevant formula below.

A Non-reversing peak torque Selection torque [Nm] = System peak torque

Selection torque [Nm] =

 System peak kW × 9 550 ––––––––––––––––––––– r/min

B Reversing high peak torque Selection torque [Nm] =

 1 .5 × system peak torque –––––––––––––––––––––– r/min

#### C Occasional peak torques (non-reversing)

If a system peak torque occurs less than 1 000 times during the expected coupling life, use the following formula:

Selection torque [Nm] =  $0.5 \times$  system peak torque

or

Selection torque [Nm] =

0.5 × system peak kW × 9 550 r/min

#### 2 Brake applications

If the torque rating of the brake exceeds the motor torque, use the brake rating as follows:

Selection torque [Nm] = Brake torque rating × Service factor.

#### Formula selection example High peak load

Select a coupling for reversing service to connect a gear drive low speed shaft to a metal forming mill drive . The electric motor rating is 30 kW and the system peak torque estimated to be 9 000 Nm. Coupling speed is 66 r/min at the motor base speed. The drive shaft diameter is 90 mm. The metal forming mill drive shaft diameter is 120 mm.

#### 1 Type

Refer to pages 6 and 7 and select the appropriate coupling type.

2 Required minimum coupling rating Use the reversing high peak torque formula in step 1B.

 $1.5 \times 9000$  Nm = 13 500 Nm = Selection torque

#### 3 Size

From product table on page 30, size 35 with a torque rating of 18 500 exceeds the selection torque of 13 500 Nm.

#### 4 Other considerations

Gear coupling size 35 has a maximum bore capacity of 124 mm from product table on page 30 and the allowable speed of 3 900 r/min exceeds the equipment requirements .

#### Formula method for brake disc applications

To determine the capacity required for a dynamic brake application:

$$
(1a) M_{TB} = \frac{kW \times 60 \times 10^3}{2 \times \pi \text{ r/min}} = x 2.0 \text{ [Nm]}
$$

which may be simplified to:

$$
(1b) M_{TB} = \frac{kW \times 9550}{r/min} = x 2.0 \text{ [Nm]}
$$

Additionally, where the inertias involved (I) are known or can be determined (by reference to the brake position), and the braking deceleration time, in rads/sec  $(\alpha)$ is known, the torque may also be determined from:

(1c)  $M_{TR} = 1 \times \alpha \times 2.0$  [Nm]

The coupling capacity [MT] from the catalogue must be greater than the figures obtained in 1(a), 1(b) or 1(c) above.

(2)  $M_{TNOM} \geq MTB$  [Nm]

Note: Where the brake is only being used as a holding brake, i.e. the system is brought to a stop by other means, prior to application of the brake, standard coupling selection procedures may be used.

(a) Gear coupling (double engagement) with brake disc (schematic only)  $(\rightarrow$  fig. 1).

Note: The brake disc spigot arrangement may vary from that illustrated, depending on size .

The gear coupling (double engagement<sup>1)</sup>), is shown in fig. 1 on page 24.

The symmetrical arrangement of the gear coupling allows the hubs to be on either the driveR or driveN (braked) shafts. Subject to the braking torque, the only deviation from standard gear coupling components, is the extended length of the fitted bolts. Some axial allowance is required for maintenance, as the cover need to be removed for inspection.

#### Note:

#### a. Brake disc dimensioning

- In general the coupling selection for dynamic braking should be no less than 200% of the running (installation) torque, unless the results of a full analysis of the inertias involved are known, along with the desired stopping time.
- The diameter of the brake disc (D<sub>b</sub>), will be determined from the required torque, and the caliper's force at the effective diameter ( $D_{cal}$ in fig. 1 on page 24) at which the caliper unit (or units) will engage.
- Multiple calipers, typically no more than two, are generally set 180° apart. The thickness of the disc, and whether plain or ventilated, will also be determined by
	- *–* the inertias ∑ I (kgm<sup>2</sup>) being retarded, relative to the brake position,
	- the stopping time t<sub>s</sub> (in seconds) required

#### b. Brake disc (general)

- International standards, such as DIN 15435, have tables of recommended diameters and thicknesses (or widths) for both disc and drum (shoe) type brakes . (Many brake-system manufacturers also have their own factory standards).
- Disc material will vary depending on the application, capacity and the amount of energy that is required to be dissipated during engagement. Typically however, they are made of spheroidal graphite (nodular) cast iron (e.g. DIN GGG40, AISI 60-40-18; JIS FCD400) .
- Thickness variation overall should be <0 .05 mm total, and surface finish  $≤0.002$  μm.

# <span id="page-23-0"></span>Engineering data

These maximum operating alignment limits are each based on /° per flex half coupling . Combined values of parallel and angular misalignment should not exceed /° . Type GC slide couplings are limited to /° per flex half.

Do not use single engagement couplings to compensate for parallel offset misalignment.

For additional information about gear couplings, please refer to tables 1 to 6.

#### Gear couplings gap measurement for standard and reversed hubs

In some instances it may be required to extend or shorten, the "G" or gap measurement between the hubs without the spacer option. This is usually done by either reversing both (Type 2), or one (Type 3) of the hubs.

On request, special hub dimensions (Type 4) can also be made to suit, where the hub through length ( $\mathsf{L}_1$  or  $\mathsf{L}_2$ ) is to specific requirements.

Table 1 shows the "G" (Gap) dimensions for the various configurations up to size GC70.

Data on the larger size couplings (PHE 80GC and above) is available on request. If hubs are heat-treated or made from alloy 4140 (HT), there is no dimensional variation.



# Order data

A complete gear coupling consists of: 2 hubs, 2 covers and 1 assembly kit. Coupling size 80 and above consists of: 2 hubs, 1 male cover, 1 female cover and 1 assembly kit. For more detailed information on ordering specific gear couplings, refer to table 7 on page 28.



#### Fig. 1

#### Table 1



<sup>1)</sup> Refer to SKF PTP for gap dimensions for these sizes, and above.

Misalignment capability





#### <span id="page-25-0"></span>Puller bolt hole data (gear and rigid)





Bolt data flex half







<sup>1)</sup> Bolt pitch diameters are originally based on imperial (inch) dimensions. The metric dimensions may have been rounded.<br><sup>2)</sup> Bolts are all grade 8,8 (unless otherwise specified) and to factory standard for reamed holes.

## Typical gear coupling brake rating

Table 4

#### capacities (M<sub>TMAX</sub>)



Larger sizes available on request . (Refer SKF\_PT-Inquiry)

#### Bolt data flex half





<sup>1)</sup> Bolt pitch diameters are originally based on imperial (inch) dimensions. The metric dimensions may have been rounded.<br><sup>2)</sup> Bolts are all grade 8,8 (unless otherwise specified) and to factory standard for reamed holes

#### Table 7



<sup>1)</sup> The limitations in the couplings' torque capacity, when fitted with a taper bushing, is based on the maximum recommended torque for the relevant taper bushing with a standard keyway.<br>Way.<br>For this reason it is unecono

## <span id="page-28-0"></span>Installation

The performance of the coupling depends largely upon how it is installed, aligned and maintained .

1 Mount the flanged sleeves with the seal rings before the hubs

Clean all metal parts using non-flammable solvent and check hubs, shafts and keyways for burrs and remove if necessary. Lightly coat the seals with grease and place well back on the shafts before mounting the hubs . Optionally both shafts can be lubricated with light oil or anti-seize compound. Mount the hubs on their respective shafts so that each hub face is flush with the end of the shaft unless otherwise indicated ( $\rightarrow$  fig. 1).

#### 2 Gap and angular alignment

Use a feeler gauge equal in thickness to the gap specified in table 2 on page 25 . Insert the gauge as shown in image  $(\rightarrow$  fig. 2) to the same depth at 90° intervals and measure the clearance between the gauge and hub face. The difference in the minimum and the maximum measurements must not exceed the angular limits specified in table 2 on page 25.

#### 3 Offset alignment

Align the two hubs so that a straight edge rests squarely on both hubs as in image  $(\rightarrow$  fig. 3), and also at 90 $^{\circ}$  intervals. The clearance must not exceed the parallel offset installation limits specified in table 2 on page 25. Tighten all foundation bolts ( $\rightarrow$  fig. 4) and repeat steps 2 and 3 . Realign the coupling if necessary.

4 Pack with grease and assemble the sleeves

Pack the gears of the hubs with grease . Insert the gasket between the sleeves and position the sleeves with the lubrication holes approximately 90° apart . Then push the sleeves into position and using the supplied fasteners, bolt the sleeves together. Once the coupling is assembled, remove the lubrication plugs from the sleeves . Insert a grease fitting in one of the holes and pump grease into the sleeve until it is forced out of the opposite lubrication holes (→ fig. 5). Replace the lubrication plugs. The installation is complete.



















Size 80 to 200



<sup>1)</sup> Minimum clearance required for aligning coupling.

Double engagement couplings are designed for most horizontal, close coupled applications . This coupling accommodates both offset and angular misalignment, as well as end float.

Applications include: fans, pumps, steel and paper mill drives, cranes and conveyors.<br>Bore tolerances will be K7 and key width (b) will be P9 (close fit) for coupling sizes 130 and bigger unless stated otherwise.

Weights are given, in kg, with minimum listed bore, excluding lubricant .





Size 10 to 70 Size 80 to 120

Size	Power per Rated 100 r/min torque		Speed	Bore diameter Flex hub Se hub			Dimensions											Gap	weight	<b>Lubricant Coupling</b> weight without	
			Max.	Max.	Max.	Min.	A	B	C	D	Ε	F	H	J	$K^{1}$		M <sup>2</sup>	Q	Min.		bore
	kW	Nm	r/min	mm															mm	kg	
10 GCSE	11.9	1139	8000	48	60	13	116	87	43	69	2.5	84	14	39	$\qquad \qquad -$	40	51	42	$\overline{4}$	0.02	4.5
15 GCSE	24.6	2350	6500	60	75	19	152	99	49	86	2.5	105	19	48	$\qquad \qquad -$	46	61	49	$\overline{4}$	0.04	9.1
20 GCSE	44.7	4270	5600	73	92	25	178	124	62	105	2.5	126	19	59	$\overline{\phantom{0}}$	58	77	61	$\overline{4}$	0.07	15.9
25 GCSE 30 GCSE 35 GCSE	78.3 127 194	7474 12 100 18500	5000 4400 3900	92 105 124	111 130 149	32 38 51	213 240 279	156 184 213.5 106	77 91	131 152 178	2.5 2.5 2.5	155 180 211	21.8 21.8 28.4	72 84 98	$\qquad \qquad -$ $\qquad \qquad -$ $\overline{\phantom{0}}$	74 88 102	92 107 130	76 90 105	5 5 6	0.12 0.18 0.27	27.2 43.1 61.2
40 GCSE	321	30 609	3600	146	171	64	318	243	121	210	4.1	245	28.4	111	$\overline{\phantom{a}}$	115	145	119	7	0.47	99.8
45 GCSE	440	42000	3200	165	194	76	346	274	135	235	4.1	274	28.4	123	$\overline{\phantom{m}}$	131	166	135	8	0.57	136.1
50 GCSE	593	56600	2900	178	222	89	389	309	153	254	5.1	306	38.1	141	$\overline{\phantom{m}}$	147	183	152	9	0.91	195.0
55 GCSE	775	74030	2650	197	248	102	425	350	168	279	5.1	334	38.1	158	$\overline{\phantom{m}}$	173	204	178	9	1.13	263.1
60 GCSE	947	90400	2450	222	267	114	457	384	188	305	6.6	366	25.4	169	$\qquad \qquad -$	186	229	193	10	1.70	324.3
70 GCSE	1420	135 000	2 1 5 0	254	305	127	527	454	221	343	8.4	425	28.4	196	$\overline{\phantom{a}}$	220	267	229	13	2.27	508
80 GCSE	1780	170 000	1750	279	343	102	591	511	249	356	$\qquad \qquad -$	572	$\overline{\phantom{m}}$	243	450.8	249	300	$\overline{\phantom{m}}$	13	4.99	698.5
90 GCSE	2360	226 000	1550	305	381	114	660	566	276	394	$\qquad \qquad -$	641	$\overline{\phantom{m}}$	265	508.0	276	327	$\overline{\phantom{0}}$	14	6.35	984.3
100 GCSE	3 2 5 0	310000	1450	343	406	127	711	626	305	445	$\overline{\phantom{a}}$	699	$\overline{\phantom{m}}$	294	530.4	305	356	$\overline{\phantom{a}}$	16	7.71	1251.9
<b>110 GCSE</b>	4320	413000	1330	387	445	140	775	682	333	495	$\qquad \qquad -$	749	$\overline{\phantom{m}}$	322	584.2	333	384	$\overline{\phantom{m}}$	16	9.07	1637.5
<b>120 GCSE</b>	5810	555000	1200	425	495	152	838	722	353	546	$\overline{\phantom{a}}$	826	$\overline{\phantom{m}}$	341	647.7	353	403	$\overline{\phantom{a}}$	16	10.89	2077.5

 $1)$  May be an "as cast" version depending on coupling size and bore.

2) Minimum clearance required for aligning coupling .

These single engagement couplings are not designed for floating shaft applications and only accommodate angular misalignment. For floating shaft applications, please, refer to page 30 and 33.



#### Size 80 to 160



<sup>1)</sup> The figures for the HT and XP are indicative only.

Applications for the HT and XP series couplings should be referred to SKF PTP for confirmation of both capacity and suitability for the specific application.<br>2) Bore tolerances will be K7 unless stated otherwise. Key width (up to and including 500 mm only) . Above 500 mm bore, keyway dimensions MUST be specified as not covered by international standards . Shallow keys, when required, will be to DIN6885/3 .

3) Weights are given in kg, with the minimum listed bore, and excluding lubricant .





<sup>1)</sup> Minimum clearance required for aligning coupling.

Double engagement spacer couplings are designed for pump and compressor applications .

The coupling consists of a standard double engagement coupling and a spacer tube which is available in various lengths .





Double engagement Slide







Type 1 Type 2 Type 2 Type 2 Type 3 Type 3





<sup>1)</sup> Minimum clearance required for aligning coupling.

Larger sizes available: contact SKF for details.

Double engagement slide couplings are designed for horizontal close coupled applications and are designed to accommodate

thermal expansion of the shaft and large mechanical vibratory screens .

These couplings are available with 3 different ranges of axial capabilities .





Type 1 Type 2

Size	Power per Rated 100 r/min torque		Speed	Bore diameter			<b>Dimensions</b>			Lubricant	Coupling weight without bore				
				Flex hub Se hub		A	C	D	F	H	J	L	weight		
			Max.	Max.	Max.	Min.									
	kW	Nm	r/min	mm										kg	
10 GCSL 15 GCSL 20 GCSL	11.9 24.6 44.7	1139 2350 4270	5300 4 3 0 0 3700	48 60 73	60 75 92	13 19 25	116 152 178	43 49 62	69 86 105	84 105 126	14 19 19	39 48 59	40 46 58	0.01 0.02 0.04	5 9 16
25 GCSL 30 GCSL 35 GCSL	78.3 127 194	7474 12 100 18 500	3300 2900 2600	92 105 124	111 130 149	32 38 51	213 240 279	77 91 106	131 152 178	155 180 211	21.8 21.8 28.4	72 84 98	74 88 102	0.06 0.11 0.18	29 43 68
40 GCSL 45 GCSL 50 GCSL	321 440 593	30 609 42000 56 600	2400 2100 1900	146 165 178	171 194 222	64 76 89	318 346 389	121 135 153	210 235 254	245 274 306	28.4 28.4 38.1	111 123 141	115 131 147	0.27 0.34 0.54	97 136 195
55 GCSL 60 GCSL 70 GCSL 1420	775 947	74 030 90 400 135 000	1800 1600 1400	197 222 254	248 267 305	102 114 127	425 457 527	168 188 221	279 305 343	334 366 425	38.1 25.4 28.4	158 169 196	173 186 220	0.73 0.96 1.36	263 324 510
Size		Type 1							Type 2						



<sup>1)</sup> Minimum clearance required for aligning coupling.

Larger sizes available: contact SKF for details.

These couplings are available with 2 different ranges of axial capabilities .




Rigid flanged sleeve couplings are designed for horizontal, close coupled applications . These are excellent high torque couplings to use where there is no need to accommodate misalignment.







Gear coupling mounting in modified hubs

Type "F" mounting  $C_1 > C_2$ <br>(standard configuration)

Type "H" mounting  $C_1 > C_2$ <br>(non-preferred, not available in all series)

Size	Taper bushing designation	<b>Bushing torque</b> capacity	Bore diameter range <sup>1)</sup>		Nominal hub length	Hub diameter
			Min.	Max.	Lb	$D_h$
	$\overline{\phantom{0}}$	Nm	mm		mm	mm
10 GCTB 15 GCTB 20 GCTB	1215 1615 2012	405 485 810	$\begin{array}{c} 13 \\ 13 \end{array}$ 13	32 42 50	43 53 62	69 88 105
25 GCTB 30 GCTB 35 GCTB	2525 3030 3535	1275 2710 5060	25 24 32	65 80 91	77 91 107	131 152 178
40 GCTB	4040	8727	37	103	121	210

 $1)$  The taper bushing combination may be used in full flex-flex or flex-rigid configuration. Check rigid hub dimensions on page 35.

# Floating shaft gear couplings

The SKF floating shaft coupling consists of two standard single engagement couplings, two gap discs and a connector shaft.

A floating shaft can eliminate the requirement for additional bearing supports along the spanning shaft because the shaft is supported at the ends by connected equipment through the single engagement couplings.

## Flex hubs on floating shafts

Assembly of the flex hubs on the floating shaft allows for easier replacement in case of coupling wear and allows the rigid hubs with their larger bore capacities to be used on the connected equipment shafts . This often allows for smaller coupling sizes in the design. See drawings on page 42.

## Rigid hubs on floating shaft

When the rigid hubs are on the floating shaft, shorter shaft spans can be used since no cover drawback is required. Since the flex hubs are on the outboard side, the points of articulation are further apart, thus allowing for greater offset misalignment. See drawings on page 42.

#### Floating shaft data

Size Assembly SB diameter SD diameter Maximum DBSE for r/min



Assembly torque ratings are limited by the coupling size, shaft end diameter or both.<br>Interpolate for intermediate speeds. The maximum DBSE is based on 70% of the critical speed.



**SKF** 

Table 1

## Solid floating shaft selection

Single engagement type GCSE and GC-SEV couplings are used with floating shafts in either horizontal or vertical applications . For vertical applications, select a type V coupling for the lower assembly. Select floating shaft couplings as follows:

- 1 Use the standard or formula selection methods and see product tables on page 41 and 44 to select the coupling. Record the system torque from the standard method or the selection torque from formula method.
- 2 Select the shaft diameter from product tables on pages 41 and 42 that has an assembly torque rating equal to or greater than the system or the selection torque determined in the coupling selection.
- 3 Check the maximum "DBSE" for the shaft diameter you selected and the running speed for the shaft length required from product tables on page 41 and 44 . Refer to the graph in diagram 1 on page 39 to determine if the shaft requires balancing.
- 4 If the application shaft length exceeds the maximum "DBSE" listed, select the next larger shaft diameter or the next larger size coupling.









Flex hubs on floating shaft (RFFR)



Rigid hubs on floating shaft (FRRF)



# Disc couplings

The SKF disc coupling is the ideal solution in medium to high torque applications that require torsional rigidity, offer some allowance for misalignment, and do not require lubrication . These applications typically have a capacity range up to 178 kNm in a range of configurations including single disc, double disc, and spacer for both horizontal and vertical mounting. Standard shaft capacities are up to 289 mm.

The SKF disc coupling consists of two hubs and a laminated stainless steel disc pack secured by a series of fitted bolts retained by nylon insert lock nut nuts.

For spacer units, the spacer length is held between two disc pack sets.

Single disc units can accommodate angular  $(\alpha)$  offset only. Double disc pack units, with a spacer, will allow for angular  $(\alpha)$ , parallel  $(\delta)$ , or combined offset. Both configurations will also allow for some axial (δ) movement.

The disc pack, or spacer may be removed and re-installed radially, meaning the prime mover and driven machine need not be moved at all.

The all-steel machined components allow for high speed applications to be handled with ease. With two-plane dynamic balancing, higher speeds are often permissible.

Hubs are carried with pilot bores so that boring to requirements is easy . In addition, where zero backlash is required, the use of the SKF FX Keyless Bushing is a simple and economical solution.

#### The SKF Disc Coupling offers the following benefits:

- Medium to high torque capability
- Cost effective (v torque and size)
- No lubrication required
- No frictional or energy losses
- Quiet operation (no meshing)
- Zero backlash
- Angular misalignment  $(\alpha^c)$
- Parallel offset  $(\beta)$  with spacer / double disc pack configuration only
- High speed capability (may require dynamic balancing over 50 m/s)
- Limited end-float / axial movement (δ)
- Temperature-tolerant (generally up to 250 °C)
- Low inertia / mass MK2 (when compared with other metallic-type couplings)
- Various hub designs, including short or inverted hub
- Standard spacer lengths to ANSI and ISO standards generally available
- Available with longer tubular spacers (steel or composite in some instances)
- Ease of mounting / alignment and maintenance

#### Coupling types

The SKF Disc Coupling is available in 2 basic configurations:

- Single disc
- Double disc
	- *–* Short spacer
	- *–* Standard spacer
	- *–* Custom spacer
	- *–* Floating horizontal
	- *–* Floating vertical

## Selection

### Standard selection method

This selection method can be used for most motor, turbine or engine-driven applications, with appropriate service and duty factors.

The following information is required to select an appropriate SKF Disc Coupling:

- Power (kW)
- Speed (r/min)
- Torque (Nm)
- Type of driven equipment
- Application and duty cycle
- Shaft diameters (or at least the maximum bore)
- Shaft gap (DBSE)
- Space limitations (if any)
- Other ambient conditions, such as *–* temperature
	- *–* adverse environment

Where applications involve reversing or braking torque, please contact your local SKF technical expert for assessment.

1 Determine the torque of the system, using Formulae 1.1

$$
M_T = \frac{kW \times 9550}{r/min}
$$

where

 $M_T$ <br>kW Torque (moment) [Nm] Motor or demand power (kW) r/min Revolutions per minute [min–1]

- 2 From the service factor tables (**†** page 87), select a suitable service factor (F $_{\rm S}$ ) for the application.
- 3 Determine the minimum torque requirement (MC) for the coupling by multiplying the torque determined in (1), by the service factor selected in  $(2)$ :

$$
M_C = M_T \times F_S
$$

The coupling must have a torque capacity equal to or greater than this resultant M<sub>C</sub> figure.

4 Check the bore size capacity for both shafts . If the bore size is too small, a larger coupling may be required to accommodate the shafts.

5 Check to make sure other parameters such as maximum permissible speed and any dimensional limitations are all met .

### Standard selection example

Select a coupling to connect a 30 kW, 1 440 r/min electric motor to a cooling tower fan (force draft) . The motor shaft is 48 mm, and the pump shaft 55 mm. A spacer type is required of approx . 4" (101.6 mm) for ease of maintenance. Maximum temperature is 60 degrees, with other space limitations. Operation is  $10-12$  hours a day.

1 Determine the torque of the system:

30 x 9 550  $M_T = \frac{1440}{1440} = 199$  Nm

- 2 Determine the service factor from page 87. For the type of application the  $F_S$  is 2.
- 3 The minimum required coupling capacity rating (M<sub>C</sub>) is 2.0 x 199 = 398 Nm .

The coupling capacity must be equal to or greater than this figure.

4 From the tables on page 50, a type PHE W4D-030 is selected. Torque capacity 774 Nm Max, shaft Dia 58 mm Spacer (standard) 102 mm Maximum r/min 7 300 r/min

5 Selection summary: Type PHE W4D-030X102MMX48X55 Complete with 102 mm spacer (standard) and hubs bored to 48 mm (H7) and 55 mm (H7) respectively.

Note: If no tolerances are given, the standard SKF bore diameter tolerances given in table 4 (**†** page 83) will be used.

Unless stated otherwise, all bores come with standard (ISO Metric, or BS INCH) keyways . In some instances a shallow key may be necessary (Metric DIN 6885/3) .

### Disc coupling series designation<sup>1)</sup>



1) The series designations shown above (columns 3, 4 and 5) should be used when a complete coupling (rather than components)

is being designated, such as the example shown in 5, *Selection summary* .

## Engineering data

For additional useful information on disc couplings, such as characteristics and applications of disc couplings. Please, refer to the following tables.

# Order data

A disc coupling exists at least of 2 hubs and 1 disc pack and bolt kit. The number of required disc pack and bolt kits depend on coupling type . Vertical kits and vertical spacer kits might also be needed. For details refer to table 4.





#### Table 4



The complete coupling designation consists of the series, size and bore details. If bore is not specified, solid bore (RSB) is supplied, for example: PHE W6D-35x50MMx50MM or<br>PHE W6D-45x350MMx50x50MM, where 350 mm is the re

#### Disc laminate swagging





## Installation

1 Clean all metal components . Remove burrs from flange bores and ensure keyways are clean.

#### 2 Shaft projection length

When the distance between the ends of the shaft is less than "G", adjust the flange placement on the shaft to recommended dimension "G". This can be done by projecting the shaft  $(\rightarrow$  fig. 1).

If shaft projection into the element zone is required, please refer to table 2 on page 45 for maximum diameter for each size element.

The maximum projection for shafts larger than the stated allowance is listed in table 2 on page 45, dimension "S". The projections ensure that the shaft does not interfere with the disc element.

#### 3 Alignment

Using the dial gauge, check the coupling installation alignment for accuracy, both angular  $(α)$  and parallel offset  $(\Delta)$ .

A Checking for angular misalignment.  $(\rightarrow$  fig. 2).

To conduct an angular misalignment check, fix the dial gauge on one hub and rotate the hub to find the minimum reading . Then set the gauge to zero.

Take extra care to measure the deflection away from the through holes, as they may be slightly distorted from machine work . Check deflection at the smoothest unbroken area . Refer to table 3 for deflection of 0.1 degree.

B Checking for parallel misalignment. Check parallel alignment by using a dial gauge ( $\rightarrow$  fig. 3).

An accuracy reading should be taken as the shaft is rotated. Any parallel misalignment will produce an equivalent angle in floating shaft couplings, or where there is a large distance between shafts.

Note: Misalignment of 2 mm parallel per 1 000 mm distance between flanges results in 1 degree angular misalignment.

#### 4 Coupling assembly

As shown in the exploded view diagram  $(\rightarrow$  fig. 4), the coupling is assembled completely from supplied parts. It is important to take extra care when fitting the bolts, as forcing them through may damage the thick washer and result in protrusion.

Fasten all the nylon insert lock nut nuts to the required torque, as shown in the relevant disc coupling ratings tables .

The correct torque will ensure that the coupling operates smoothly. Alternate the projection of bolt heads and nuts for the best possible transmission and balance.

#### 5 Running of the couplings

To ensure longest possible service life, the coupling should be rechecked for both angular( $\alpha$ ) and parallel ( $\Delta$ ) misalignment,one to two hours after initial start-up.

At the same time, it is also necessary to check and re-tighten the bolts to the tightening torque shown in the relevant dimension tables . The nylon insert lock nut nuts can be re-fastened up to 10 times, after which , replacement is recommended.

The bolts supplied with the coupling are special machined fitted bolts, with tolerances to ensure the best possible fit.

Note: Do not replace with standard commercial bolts, as looseness and imbalance may occur.

Any damage to the stainless disc element pack requires immediate replacement.



Fig. 2

 $Fig. 1$ 















1) If higher speed required, contact SKF<br><sup>2)</sup> For dimension C in type 4F, this varies depending on spacer length<br><sup>3)</sup> For coupling weight in type 4F, this varies depending on spacer length







 $^{\rm 1)}$  Higher speeds may be permissible if system is dynamically balanced (with finished bores only)

<sup>2)</sup> For dimension C in type 4F, this varies depending on spacer length<br><sup>3)</sup> For coupling weight in type 4F, this varies depending on spacer length<br><sup>4)</sup> Preferred standard spacer lengths to both ISO and ANSI standards are







- 
- <sup>2)</sup> For dimensions B, C in type 6F, this varies depending on spacer length<br><sup>3)</sup> For coupling weight in type 4F, this varies depending on spacer length<br><sup>4)</sup> Preferred standard spacer lengths to both ISO and ANSI standards







 $^{\rm 1)}$  Higher speeds may be permissible if system is dynamically balanced (with finished bores only)

- 
- <sup>2)</sup> For dimension C in type 4F, this varies depending on spacer length<br><sup>3)</sup> For coupling weight in type 4F, this varies depending on spacer length<br><sup>4)</sup> Preferred standard spacer lengths to both ISO and ANSI standards are

## Floating shaft disc couplings

SKF Floating shaft disc couplings transmit power between widely separated machine shafts, or where large parallel misalignment exists.

Allowable rotational speeds are determined, and limited, by the span and the balance condition of the coupling system.

Balancing is necessary for high speeds and long shafts as indicated in the following tables 1 to 3.

Disc floating shaft couplings are also available for vertical applications with the addition of a vertical floating shaft kit .

- 1 Do not use floating shaft couplings with long, overhanging shafts.
- 2 Consult SKF for spans greater than 6 000 mm, or for speeds in excess of those indicated in the tables .





For BE dimensions over 6 000 mm, please contact SKF Floating shaft couplings should not be used with long overhang shafts



For BE dimensions over 6 000 mm, please contact SKF Floating shaft couplings should not be used with long overhang shafts



For BE dimensions over 6 000 mm, please contact SKF Floating shaft couplings should not be used with long overhang shafts

Table 2





<sup>1)</sup> Maximum rotational speed (r/min) is based on parallel misalignment no more than 2/1 000<br><sup>2)</sup> Rated torque is a maximum figure<br><sup>3)</sup> For BE dimensions over 6 000 mm, please contact SKF





1) Maximum rotational speed (r/min) is based on parallel misalignment no more than 2/1 000 2) Rated torque is a maximum figure





1) Maximum rotational speed (r/min) is based on parallel misalignment no more than 2/1 000 2) Rated torque is a maximum figure

<sup>3)</sup> The actual BE value will be determined by the customer<br><sup>4)</sup> For BE dimensions over 6 000 mm, please contact SKF

Floating shaft couplings should not be used with long overhang shafts

# Flex couplings

SKF Flex Couplings are designed to accommodate misalignment and shock loads and dampen vibration levels. These easy to install, maintenance-free couplings are available with either a machined-to-size or tapered bore.

Couplings with a tapered bore can be Face (F) mounted or Hub (H) mounted . The more versatile Reversible (R) design can be either face or hub mounted depending on the application . These couplings are also available with a taper bushing.

SKF Flex Couplings consist of 2 flanges and 1 tyre . The flanges are phosphate coated for improved corrosion resistance . The addition of a standard sized spacer flange can be used to accommodate applications where it is advantageous to move either shaft axially without disturbing either driving or driven machines.

SKF Flex tyres are available in natural rubber compounds for applications ranging from  $-50$  to  $+50$  °C. Chloroprene rubber compounds should be used in applications where exposure to greases and oils are likely . These compounds can accommodate temperatures ranging from  $-15$  to  $+70$  °C. The chloroprene tyres should be used where fire-resistance and anti-static (F.R.A.S.) properties are required.

## Selection

#### 1 Service factor

Determine the required service factor from tables 9 and 10 on pages 87 and 88 .

#### 2 Design power

Multiply the normal running power by the service factor. This gives the design power for coupling selection.

#### 3 Coupling size

Using the data from table 1 on page 60, find the speed rating for a coupling that has a power that is greater than the design power . The required SKF Flex coupling is listed at the head of the column.

#### 4 Bore size

Using product tables on page 63 and 66, check if the chosen flanges can accommodate both the driving and driven shafts .

## Example

A SKF Flex coupling is required to transmit 30 kW from an electric motor running at 1 440 r/min to a centrifugal pump for 14 hours per day . The diameter of the motor shaft is 30 mm. The diameter of the pump shaft is 25 mm. A tapered bore is required.

#### 1 Service factor

The appropriate service factor is 1. See tables 9 and 10 on pages 87 and 88.

2 Design power Design power =  $30 \text{ 1} = 30 \text{ kW}$ 

#### 3 Coupling size

By searching for 1 440 r/min in table 1 on page 60, the first power figure to exceed the required 30 kW in step (2) is 37.70 kW. The size of the coupling is  $70$ 

#### 4 Bore size

By referring to product tables on page 63 and 66, it can be seen that both shaft diameters fall within the bore range available. Please note that for this coupling the bore sizes for the Face and Hub design are different.



Table 2



# Engineering data

## Power ratings

Maximum torque figures should be treated as short duration overload ratings occurring in circumstances such as direct-on-line starting.

For speeds not shown, calculate the nominal torque for the design application using the formula below and select a coupling based on the nominal torque ratings.

Nominal torque (Nm) =

Design power (kW)  $\times$  9 550 ––––––––––––––––––––––––

r/min

For additional information about SKF Flex Couplings, see table 1 and 2 on page 60.

# Order data

A complete SKF Flex coupling consists of: 2 flanges and 1 tyre.

For additional information about ordering a coupling see table 3.



1) To complete designation add distance between shaft ends. PHE SM25-100DBSE.

An SKF Flex coupling consists of 2 flanges and 1 tyre. An SKF Flex Spacer Coupling consists of 2 flanges, 1 tyre and 1 spacer (spacer part number consists of spacer shaft and rigid flange).

# Installation

- 1 All metal components should be cleaned. Be sure to remove the protective coating on the flange bores. The taper bushings should be placed into the flanges and the screws lightly tightened.
- 2 If internal clamping rings are being used (size 40–60), position them onto the shaft  $(\rightarrow$  fig. 1). Place the flanges next to the clamping ring on each shaft and position them so that dimension M is obtained between the flange faces ( $\rightarrow$  table 4).

Where taper bushings are used, see separate fitting instructions supplied with the taper bushings.

Flanges with external clamping rings (sizes 70–250) should have the clamping rings fitted when installing, engaging only two or three of the threads of each screw at this time. These flanges should be positioned so that M is obtained by measuring the gap between the flange faces.

3 If shaft end float is to occur, locate the shafts at mid-position of end float when checking dimension M. Note that shaft ends may project beyond the faces of

the flanges if required. In these cases, allow sufficient space between shaft ends for end float and misalignment.

4 Parallel alignment should be checked by placing a straight edge across the flanges at various points around the circumference ( $\rightarrow$  fig. 3). Angular alignment is checked by measuring the gap between the flanges at several positions around the circumference . Align the coupling as accurately as possible, particularly on highspeed applications.



- 5 Spread the tyre side walls apart and fit over the coupling flanges, making sure that the tyre beads seat properly on the flanges and clamping rings . To make sure that the tyre sits properly in position, it may be necessary to strike the outside diameter of the tyre with a small mallet  $(\rightarrow$  fig. 4). When the tyre is correctly positioned there, should be a gap between the ends of the tyre as shown in table  $5 \rightarrow$  fig. 5).
- 6 Tighten clamping ring screws (**→ fig. 6**) alternately and evenly (half turn at a time), working round each flange until the required screw torque is achieved (**†** table 4) .



Hexagon socket caphead clamping screws on these sizes















Min. Max.



Size Type Bushing number Mass Inertia Designation Tyre-designation<br>Natural Natural Bore Types F and HType B Key Natural F .R .A .S

screw<br>OD L E L E <sup>SCrew</sup> OD FD H F R<sup>1)</sup> G<sup>2)</sup> M



<sup>1)</sup> Is the clearance required to allow tightening of the clamping screws and the tapered bushing. Use of a shortened wrench will reduce this dimension.<br><sup>2)</sup> The amount by which the clamping screws need to be withdrawn to

For coupling sizes 70, 80, 100 and 120 "F" flanges require a larger bushing than "H" flanges .

Mass and inertia figures are for a single flange with midrange bore and include clamping ring, screws, washers and half tyre .

# Flex spacer coupling

The SKF Flex coupling spacer is used to join two shaft ends that cannot be positioned close enough to just use a coupling alone.

The spacer also allows removal of a shaft without the need to move either the driving or the driven machine. For example, this allows easy and fast replacement of impellers in pump applications.

# Installation

- 1 Place each tapered bushing in the correct flange and tighten the screws lightly.
- 2 If keys are being used, side fitting keys with top clearance should be used.
- 3 Use a straight edge to align the face of the clamping ring for coupling sizes F40–F60 (→ fig. 1a) or the flange for coupling sizes F70–F250 (→ fig. 1b) with the shaft end. A dial indicator can be used to check that the runout of the spacer flange is within limits indicated in fig. 1a and b.

Position the SKF Flex flange on the spacer flange shaft to dimension "Y" shown in table 7 and secure it with a tapered bushing . This will allow for "M" and DBSE dimensions ( $\rightarrow$  fig. 1c) to be maintained when assembling. If necessary, the distance between shaft ends (DBSE) may be extended . The maximum DBSE possible is achieved when the spacer shaft end and driven shaft end are flush with the face of their respective tapered bushings.

4 Position the spacer sub-assembly in line with the spacer flange ( $\rightarrow$  fig. 1d), engage spigot align holes and insert screws. The torque values are given in table 8. Spread the tyre side walls apart and fit over the coupling flanges making sure that the tyre beads seat properly on the flanges and clamping rings.

To make sure that the tyre sits properly in position, it may be necessary to strike the outside diameter of the tyre with a small mallet. When the tyre is correctly positioned, there should be a gap between the ends of the tyre as shown in table 5.

5 Tighten the clamping ring screws alternately and evenly (half turn at a time), working around each flange until the required screw torque is achieved, as indicated in table 8.

## To dismantle

- 1 Place a support underneath the spacer sub-assembly to prevent it from falling.
- 2 Remove clamping ring screws evenly (half turn per screw at a time) to prevent the clamping rings from distorting.
- 3 When the clamping rings are loose, remove the tyre. Then remove the remaining screws and spacer.



Alignment of flanges

## Table 6







#### SKF Flex Spacer Coupling





- 
- 1) "B" Flange must be used to fit spacer shaft 2) "F" Flange must be used to fit spacer shaft

# Chain couplings

Chain couplings are able to transmit higher torque than their shafts, making them ideal for high torque applications. Available with a pilot bore, finished bore or taper bushing (face or hub), flanges are linked together with duplex roller chains enabling them to accommodate up to 2° of misalignment.

To help provide maximum service life and reliability, particularly for high speed applications, SKF recommends fitting all chain couplings with a cover and lubricating them properly . If a chain coupling is to be subjected to reversing operations, shock or pulsating loads, or other severe operating conditions, select a coupling one size larger than normal.

# Selection

## Standard selection method

This selection procedure can be used for most motor, turbine, or engine driven applications . The following information is required to select an SKF chain coupling:

- Torque power [kW]
- Input speed [r/min]
- Type of equipment and application
- Shaft diameters
- Physical space limitations
- Special bore or finish requirements

#### 1 Service factor Determine the service factor from tables 9 and 10 on pages 87 and 88.

2 Design capacity

Calculate the torque requirement for the application and service factor (SF) from the following formula:

Nominal torque (Nm) =

Design power (kW)  $\times$  9 550  $\breve{-}\times$ SF r/min

Using table 3 on page 68,

- a) Select the coupling with sufficient torque capacity.
- b) Check the coupling size selected has sufficient capacity for the shaft diameters . If not the next size up may be required to accommo date the bores.
- c) Finally recheck max. rpm, if applicable.
- 3 Size

Select the appropriate coupling from the product table on page 70 and check that chosen flanges can accommodate both driven and driving shafts.

4 Other considerations Possible other restrictions might be speed [r/min], bore and dimensions.

## Example

Select a coupling to connect a 30 kW, 1 500 r/min electric motor driving a boiler feed pump. The motor shaft diameter is 55 mm and the pump shaft diameter 45 mm . Shaft extensions are 140 mm and 110 mm respectively. The selection is replacing a gear type coupling.

- 1 Service factor From table 9 on page  $87 = 1.50$
- 2 Required design power:  $1.5 \times 30$  kW = 45 kW

#### 3 Coupling size

Look under 1 500 r/min in table 1 on page 68 and choose the first power figure which exceeds the required 45 kW . This is 95 .2 kW of coupling size 6018.

By referring to the product table on page 70, it can be seen that both shaft diameters fall within the bore range available.

#### 4 Other considerations

The speed capacity of 3 000 r/min (coupling size 6018) exceeds the required speed of 1 500 r/min . The maximum bore capacity of 62 mm exceeds the required shaft diameters of 55 mm and 45 mm . The resulting service factor is 2.11. This will provide a very good service life for the coupling and a high level of reliability.

# Engineering data

## Power ratings

Maximum torque figures should be treated as short duration overload ratings occurring in circumstances such as direct-on-line starting.

For speeds not shown, calculate the nominal torque for the application using the following formula and select a coupling according to nominal torque ratings.

Nominal torque (Nm) =

Design power (kW) × 9 550 ––––––––––––––––––––––––

r/min

For additional information about chain couplings, such as chain cover data, please refer to table 1 and 2.





Type Frequency 1 Grease monthly 2 Grease weekly . or use with cover 3 Use with fully grease-packed cover





 $^{\rm 1)}$  The maximum speeds indicated are for the couplings operating with covers installed.<br><sup>2)</sup> Items are on request only, and may be subject to minimum order quantity

Table 2

# Order data

A complete chain coupling consists of: 2 hubs, 1 chain and 1 cover.

For additional information about ordering specific couplings, refer to table 3.

# Installation

#### 1 Cleaning

Clean all metal parts using non-flammable solvent and check hubs, shafts and keyways for burrs and remove if necessary . Mount the oil seal rings on the sprocket hubs. Install the sprocket hubs flush with the end of the shafts  $(\rightarrow$  fig. 1).

#### 2 Gap and angular alignment

Measure the gap at various intervals and adjust to the "C" dimension specified in the product table on page 70. The measurement must not exceed a difference between points of more than 1° which is the allowable angular misalignment.





#### 3 Offset alignment

Align the two hubs so that a straight edge rests squarely on both hubs (→ fig. 2). Repeat this at 90° intervals. Clearance must not exceed allowable offset misalignment of 2% of the chain pitch. Tighten all foundation bolts and repeat steps 2 and 3. Realign the coupling if necessary.

#### 4 Lubrication

Lubricate the chain with grease . Wrap the chain around the two sprocket hubs and fix with the pin  $(\rightarrow$  fig. 3). Fill the cover halves with grease and insert the gaskets, install the cover and the installation is complete  $(\rightarrow$  fig. 4).



Fig. 2





Fig. 4











 $^{\rm 1)}$  Indicates according to JIS standard (with ANSI chain)<br><sup>2)</sup> Items are on request only, and may be subject to minimum order quantity

Components on the ISO (IS) and JIS series of chain couplings are not interchangeable



Assembly configuration FF Taper bushes internally mounted FTB + FTB (preferred)





Assembly configuration FH

Assembly configuration HH

Taper bushes externally mounted HTB + HTB

1 x Taper bush internally mounted 1 x Taper bush externally mounted FTB + HTB



1) Indicates according to JIS standard (with ANSI chain)

Larger sizes are available on request, and are subject to minimum order quantity

Max . RPM stated is for couplings with covers and correctly lubricated . Without covers recommended max . speeds are approx . 20% of the given speeds . Important note: As above couplings with taper-bush mounting have reduced torque capacity to that of the relevant taper bush . Check capacities .
# FRC couplings

With a higher load capacity than jaw couplings and maintenance-free operation, FRC couplings are designed as a general purpose coupling. They are able to cushion moderate shock loads, dampen low levels of vibration and accommodate incidental misalignment. FRC couplings offer a range of hubs and elements to select, to meet the demand for low cost, general purpose flexible coupling.

FRC couplings are phosphate coated for improved corrosion resistance and available with fire-resistant and anti-static elements (F.R.A.S.) FRC couplings are available with a pilot bore, finished bore or taper bushing (face or hub) to make installation quick and simple.

Fully machined outside surfaces allow alignment with a simple straight edge. Shaft connections are "fail safe" due to their interlocking jaw design.

## Selection

#### 1 Service factor

Determine the required service factor from tables 9 and 10 on pages 87 and 88 .

#### 2 Design power

Multiply normal running power by the service factor. This gives the design power for coupling selection.

3 Coupling size

Using FRC table 1 to find the speed rating for a coupling that has a power that is greater than the design power . The required FRC coupling is listed at the head of the column.

#### 4 Bore size

Using the FRC product table on page 74, check that the selected flanges can accommodate both the drive and driven shafts.

#### Example

An FRC coupling is required to transmit 15 kW from an electric motor running at 500 r/min to a rotary pump for 15 hours per day. The shaft diameter of the motor is 25 mm and the shaft diameter of the pump is 20 mm .

Table 1

1 Service factor

From table 9 on page  $87 = 1.75$ .

2 Design power  $15 \times 1.75 = 26.25$  kW



## 3 Coupling size

Search for 500 r/min in table 1 on page 71 and choose the first power figure which exceeds the required 26.25 kW. This is 31.41 kW of coupling size 150.

#### 4 Bore size

By referring to product table on page 74, it can be seen that both shaft diameters fall within the bore range available.

## Engineering data

### Power ratings

Maximum torque figures should be treated as short duration overload ratings occurring in circumstances such as direct-on-line starting.

For speeds not shown, calculate the nominal torque for the design application using the formula below and select a coupling based on the nominal torque rating.

Nominal torque  $(Nm)$  =

#### Design power (kW) × 9 550 ––––––––––––––––––––––––

r/min

For additional information on FRC couplings, refer to tables 1 and 2.

## Order data

A complete FRC coupling consists of: 2 hubs and 1 element.

For more detailed information on ordering specific couplings, refer to table 3.

#### Assembled dimensions and charachteristics



 $1)$  Mass is for an FF, FH or HH coupling with mid range tapered bushings.



NR = Natural rubber FR = Fire-resistant and anti-static (FRAS)

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Table 3

Table 2

## Installation

- 1 Place the couplings on their shafts so that shaft ends do not protrude into the internal section of the coupling. Then tighten the screws on the taper bushing to the torque values listed in the mounting instructions  $(\rightarrow$  fig. 1).
- 2 Insert the coupling element into one side of the coupling  $(\rightarrow$  fig. 2).
- 3 Move the other coupling into position and connect the two halves  $(\rightarrow$  fig. 4). Check that the assembled length is correct  $(\rightarrow$  fig. 5).
- 4 Check angular misalignment by measuring the assembled length in four positions at 90° around the coupling. Then check for parallel misalignment using a straight edge across the length of the coupling flange ( $\rightarrow$  fig. 6). Allowable angular misalignment for all FRC couplings is  $1^\circ$ .

Allowable parallel misalignment for FRC couplings is based on size (**†** table 4) .

Note: For the most consistent results, check across at least 3 of the 6 points where the rubber elements are visible between the flanges.

## Table 4

Allowable parallel misalignment Coupling size









Fig. 3



Fig. 5







Type B Type F Type H



## Jaw couplings

Jaw couplings provide a cost-effective solution for standard power applications, cushioning moderate shock loads and dampening low vibration levels.

Maintenance-free and easy to install, jaw couplings are available with a "snap wrap" element allowing element replacement in situ.

Urethane and hytrel elements have a greater power rating than nitrile elements and are recommended for applications where a compact, high torque solution is required.

## Selection

1 Service factor

Determine the required service factor in tables tables 9 and 10 on pages 87 and 88.

#### 2 Design power

Multiply normal running power by the service factor. This gives the design power for selecting a coupling with a nitrile element.

#### 3 Alternative elements

To allow coupling selection based on one power rating table (nitrile), an element correction is required to give a new reference design power . This is done by dividing the design power calculated for a nitrile element by the alternative element power factor listed in table 1.

#### 4 Coupling size

Using table 2 on page 76, search for the appropriate speed until a power greater than the design power is found. The required jaw coupling is given at the head of the column.

#### 5 Bore size

Using prodcut table on page 78, check that the selected flanges can accommodate both the drive and driven shaft .

#### Example

A jaw coupling is required to transmit 4 kW from an electric motor running at 300 r/min to a centrifugal fan for 12 hours per day. The motor shaft is 20 mm diameter and the pump shaft diameter 18 mm .

1 Service factor From table 9 on page  $87 = 1.0$ .

2 Design power Design power =  $4 \times 1.0 = 4$  kW

3 Coupling size

When looking for for 300 r/min in table 2 on page 76, the first power figure to exceed the required 4 kW of step 2 is 4.7 kW. In this case, a nitrile element can be used with a jaw coupling size 150.

4 Bore size

By referring to the product table on page 78, it can be seen that both shaft diameters fall within the bore range available.

## Engineering data

#### Power ratings

Maximum torque figures should be treated as short duration overload ratings occurring in circumstances such as direct-on-line starting .

For speeds not shown, calculate the nominal torque for the design application using the formula below and select



Table 1

coupling according to nominal torque ratings.

Nominal torque (Nm) =

Design power (kW)  $\times$  9 550 –––––––––––––––––––––––– r/min

For additional useful information on jaw couplings, such as standard bore and keyway data, please refer to tables  $1$  to  $3$ .

## Order data

A complete jaw coupling consists of: 2 hubs and 1 element. A complete coupling with spacer consists of 2 hubs, 2 nitrile wrap elements, 2 ring kits and 1 spacer.

For more detailed information on ordering specific couplings, refer to table 4.







NR = Nitrile<br>UR = Urethane<br>HL = Hytrel

Available spacer shaft lengths are 100 mm and 140 mm. To complete the designation, add spacer length. For example: PHE L090X100SPACER for spacer of 100 mm, coupling size 090.<br>When ordering bored to size and keywayed hubs,

Table 3

Table 4

Standard bore and keyway chart



## Installation

- 1 Place each coupling on its shaft so that shaft ends do not protrude into the internal section of the coupling (→ fig. 1). Then tighten the set screws.
- 2 Insert the coupling element into one side of the coupling  $(\rightarrow$  fig. 2).
- 3 Move the other coupling side into position and connect the two halves (→ fig. 3). Check that the assembled length is correct ( $\rightarrow$  fig. 4).
- 4 Check the angular misalignment by checking the assembled length in four

positions at 90° around the coupling. Check parallel misalignment using a straight edge across the length of the coupling flange ( $\rightarrow$  fig. 5). Allowable angular misalignment for all jaw couplings is 1° . Allowable parallel misalignment for all jaw couplings is 0.38 mm.

Note: For most consistent results, check across at least 3 of the 6 points where the rubber elements are visible between the flanges.





Fig. 2



Fig. 3



Fig. 4



Fig. 5





Hub Spacer



DBSE = Distance between shaft ends

Hub material is high grade cast iron. Spacer material is aluminium.

# Universal joints

Universal joints, also known as pin and block couplings, are commonly used for low to medium torque industrial, offroad and agricultural applications.

These couplings offer an economical solution for applications up to 1 800 r/min and will provide working angles of up to 25° or 35° for manual drives . SKF offers these couplings with a solid bore from stock, bored to size, square, hexagonal and round bores on request. The couplings are available in either a single (UJMA) or double (UJMB) configuration.

## Selection

Universal joints are selected based on torque. The following application information is required:

- Torque power [kW]
- Speed [r/min]
- Joint angle [°]

The product tables on page 80 provide maximum allowable torque (expressed in Nm) based on a 10° angle of inclination and continuous use.

However, if the inclination angle is not 10°, the values shown will be reduced or increased in accordance with the torque factors listed in table 1.

Torque is calculated using the following formula:

Nominal torque (Nm) =

Design power (kW) × 9 550 ––––––––––––––––––––––––

r/min

#### Example

An electric motor is driving a small gearbox . The application has the following basic data .

- Power =  $3$  kW
- Speed =  $1500$  r/min
- Joint angle = 20°
- 1 Determine the basic required torque

 3 kW × 9 550  $=19.1$  Nm 1 500 r/min

2 Adjust the torque value to accommodate

a 20° angle of inclination. Table 1 lists a correction value of 0.75. The previously calculated basic torque rating must be divided by the correction factor in order to get the adjusted torque value. In other words, a joint with larger dimensions must be selected as the angle is greater than 10° .

 19 .1 kW  $= 24.46$  Nm 0 .75 kg/m

3 From product table on page 80, the joint size UJMA13 is the proper selection.

## Engineering data

For additional information about universal joints, refer to table 1.

## Order data

Standard universal joints are without bore .

For addtional information about ordering specific universal joints, refer to table 2 .

Table 1





Available on request with finish bore, finish bore with keyway, hexagonal bore or square bore, e.g. the designations as shown below.

Universal joints with finish bore H7, with keyway (BSX30MM) – PHE UJMB45BSX30MM Universal joints with finish bore H7, without keyway (X30MM) – PHE UJMB45X30MM Universal joints with hexagonal bore (HBX30MM)

– PHE UJMB45HBX30MM Universal joints with square bore (SBX30MM) – PHE UJMB45SBX30MM

#### Single universal joints

 $\dot{D}$ 





Standard is without bore.

Available on request with finish bore H7 – on request with keyway (B), hexagonal bore (H) or square bore (Q)

#### Double universal joints





Available on request with finish bore H7 – on request with keyway (B), hexagonal bore (H) or square bore (Q)

## General engineering data on SKF couplings

## Keyseat dimensions – metric, British standard (inch) and ANSI

#### Metric DIN 6885, Part I (Standard) and Part 3 (Shallow)







Metric keyway designation should be width x depth (b x h)<br><sup>1)</sup> Tolerance range of the hub key width b is JS9.<br><sup>2)</sup> Tolerance range of the hub key width b is J9.

Table 1

#### British Imperial Standard (inch) and ANSI standard (inch)





<sup>1)</sup> For inch keyway designation should be width x depth (W x H)<br><sup>2)</sup> Tolerance each on T1 and T2 (16" to 20") is –0.000/+0.010"<br><sup>3)</sup> Tolerance each on T1 and T2 (1" to 14") is –0.000/+0.006"



<sup>1)</sup> Minimum recommended clearance above key is 0.005"<br><sup>2)</sup> Recommended tolerance on keyway width is +0.000"/-0.002"<br><sup>3)</sup> Recommended tolerance on key width is +0.002"/-0.000"<br><sup>4)</sup> A tight side-to-side fit is required bet

Table 3

#### Table 4

#### Recommended bore tolerances for SKF steel coupling hubs Shaft diameters **Bore diameter tolerances**



#### Table 5

#### Service factors per application and torque demand



#### Table 6

#### Standard (preferred) spacer lengths for respective coupling types DBSE dimension Coupling style



The figures in BOLD in the respective columns are the preferred DBSE's for the standard (ANSI or ISO) shown. The figures in (italics) are conversions, and for reference purposes only.<br>poses only.<br>The suitably of a particul

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Table 7

#### Shaft diameters and ratings for NEMA 60 Hertz







#### Service factors for chain, gear and grid couplings by application

Electric motor with standard torque

Not approved

 $1.0$ <br> $1.25$ 



For balanced opposed design, contact SKF<br>If people are occasionally transported, contact SKF for selection of the proper size coupling<br>For high peak load applications (such as metal rolling mills), contact SKF

#### Service factors for chain, gear and grid couplings by industry



For balanced opposed design, contact SKF<br>If people are occasionally transported, contact SKF for selection of the proper size coupling<br>For high peak load applications (such as metal rolling mills), contact SKF

#### Table 11

#### Service factors for disc couplings by application



#### ralues for heavy shock and fluctuating loads



#### Useful power transmission formulae

1 Power (kW) 1.1 Mechanical power  $\left[\text{kW}_{\text{M}}\right]$ 

 $kW_{M} = \frac{M_{T} x \, r/min}{9.550}$  [kW]

#### Where

 $M_T$  Torque (moment) [Nm] r/min revolutions per minute [min–1]

1.2 Electrical power  $\text{[kW}_{E}$ 

 $kW_E = \frac{\sqrt{3} \times V \times I \times \text{Cos}\phi}{1000}$  [kW]

#### Where

V Voltage (Typically 415 V for 3 ph: 240V for single ph .) I Current (amps)

cosφ Power factor (typically 0.82-0 .95 . Ref motor catalogue)

 $\sqrt{3}$  1.73 A constant for 3 phase machines of 415 V. (Ignore this for single phase machines with typically 240 V AC).

Note: To calculate the output kW, multiply the  $kW_E$  by the overall mechanical efficiency [Oξm] .

2 Torque (moment)  $[M_T]$ 2 .1 Basic formulae:

 $M_T = F \times r / Nm$ 

Where

F Force (Newtons)

r Radius of element (meters)

2.2 Power and speed known:

$$
M_T = \frac{kW \times 60 \times 10^3}{2 \times \pi \times r/min} \text{[Nm]}
$$

Where  $M<sub>T</sub>$  Torque (moment) [Nm] kW Kilowatt [kW] r/min Revolutions per minute [min–1] 9 550 is a constant, derived from: (60 x 103) / 2π

2.3 Alternatively, this may be reduced to

 $M_T = \frac{kW \times 9950}{r/min}$  [Nm]

**3** Overhung loads (radial force)  $[F_R]$ 3.1 Radial force  $[\mathsf{F}_{\mathsf{R}}]$ 

 2 x kW x 9 950  $F_R = \frac{1}{d \times r/min}$  [N]

**Where** kW Power [kW] d Pitch circle diameter – pcd – [m] r/min Revolutions per minute [min–1]

**3.2** Overhung loads  $[F_R]$ 

$$
F_R = \frac{2 \times kW \times 9.950 \times K}{dx r/min} [N]
$$

**Where** 

 $K<sub>1</sub>$  A constant, dependent on the driving element, typically For: Chain pinions  $(>19T) = 1.00$  $(14T-18T) = 1.25$  $(**13T**) = 1.40$ Gears  $(>17T) = 1.15$  $(<17T) = 1.30$ V-Pulleys  $= 1.50$ Flat belts  $= 2.50 - 3.00$ (dependent on type/construction or material)

4 Velocity (linear motion ) [m/s] 4.1 Velocity [ν]

$$
v = \frac{d \times \pi \times r/min}{60 \times 10^3} [m/s]
$$

**Where** 

- Velocity in metres per second [m/s]
- d Pitch circle diameter pcd  $-$  [mm]

(Note: If the pitch diameter is in metres, ignore the  $\times 10^3$  denominator).

**4.2** For Chain drives  $[v_1]$ 

$$
v_1 = \frac{p \times z \times r/min}{60 \times 10^3} [m/s]
$$

#### **Where**

- p Chain pitch [mm]
- z Number of sprocket teeth
- 4.3 Angular acceleration  $[\alpha]$  may be derived from the above

$$
\alpha = \frac{(v_1 - v_2)}{t} \cdot 2 \times \pi \text{ [rad/sec^2]}
$$

**Where** 

- α Angular acceleration (radians per second<sup>2</sup>)
- $v_1$ ,  $v_2$  Velocities 1 and 2 respectively [m/s]
- T Time period between the velocities  $\bm{{\mathsf{v}}}_1$  and  $\bm{{\mathsf{v}}}_2$  [sec]
- 5 Sprocket (or chain wheel) pitch diameters [ $\phi_{\rm p}$ ] **5.1** Pitch diameters  $[\phi_{\rm p}]$

$$
\phi_p = \left[\sin\frac{180}{z}\right]^{\frac{1}{2}} \text{[mm]}
$$

Where

- $\phi_{p}$  Pitch diameter [mm]
- z Number of sprocket teeth
- p Chain pitch [mm]
- sin Trig. function
- 6 Ratios [i]

$$
i = \frac{N_1}{N_2} = \frac{M_2}{M_1} = \frac{D_1}{D_2} = \frac{Z_2}{Z_1}
$$

**Where** 

- $N_1$ ,  $N_2$  Input and output speeds respectively [r/min]
- $M_1$ ,  $M_2$  Input and output torque (moment) respectively [Nm]
- $\Phi_1$ ,  $\Phi_2$  DriveR and driveN pulleys [mm or inch]
- $Z_1$ ,  $Z_2$  Number of sprocket teeth on driveR and driveN
- 7 Factors and efficiencies
	- 7.1 Gearbox efficiencies (x) (Typical only. Refer to manufacturers' tables for actual values)
		- 7 .1 .1 Helical units single reduction  $0.97$ Double reduction 0.94 Triple reduction 0.91
		- 7.1.2 Spur units single reduction 0.95 Double reduction 0.91 Triple reduction 0.88
		- 7.1.3 Worm units: For small units (centres < 150 mm), an approximation of the mechanical efficiency can be made by subtracting the ratio from  $100$ . E.g. for a  $40:1$  ratio unit, the oxm is approx. 60%

Thus, the larger the worm box centres, the more efficient (relatively) the unit.

- 7.2 V, Multi-rib and synchronous belts
	- 7 .2 .1 Standard V-belts: classical jacketed 0.94-0.97
	- 7.2.2 Raw-edge type V-belts  $0.96 - 0.98$
	- 7.2.3 Standard synchronous (Trapezoidal profile – CTB)  $0.96 - 0.97$
	- 7.2.4 High performance synchronous belts 0.97-0.98 (Curvilinear and modified curvilinear)

Note: The above belt efficiencies are based on new installations, with correctly maintained tensions.

7 .3 More common: Co-efficient of friction [μ] for different materials

#### Steel on steel:

Static friction (dry)  $\mu = 0.12 - 0.6$ Sliding friction (dry)  $\mu$  = 0.08–0.5 Static friction (greased)  $\mu$ o = 0.12–0.35 Sliding friction (greased)  $\mu$ o = 0.04–0.25

#### Wood on steel:

Static friction (dry)  $\mu$  = 0.45–0.75 Sliding friction (dry)  $\mu =$  $0.30 - 0.60$ 

#### Wood on wood:

Static friction (dry)  $\mu$  = 0.40-0.75 Sliding friction (dry)  $\mu$  =  $0.30 - 0.50$ 

#### Polymer on wood:

Static friction (dry)  $\mu$  = 0.25-0.45 Sliding friction (dry)  $\mu$  = 0.25

Steel on polymer: Static friction (dry)  $\mu$  = 0.40-0.45 Sliding friction (greased)  $\mu$  =  $0.18 - 0.35$ 

8 Common conversion factors and constants 8.1 Power [kW] Hp x 0.746 Kilowatt [kW] PS x 0.7355 Kilowatt [kW] kp m/s x 0 .0981 Kilowatt [kW] kcal/s x 4 .1868 Kilowatt [kW]

8.2 Torque (moment) [Nm] kgf-m x 9.81 Newton-metre [Nm] lbf-in x 0 .1129 Newton-metre [Nm]  $lbf-ft \times 1.36$  Newton-metre [Nm] 8 .3 Force [N] kgf x 9.81 Newton [N] lbf x 4 .45 Newton [N]  $kpx 9.81$  Newton [N] [kp = kilopond]

8.4 Pressure and stress [MN/m<sup>2</sup> or N/ mm<sup>2</sup>] pascal [Pa] 10<sup>2</sup> N/m<sup>2</sup>  $lb/in<sup>2</sup>x6.895x10<sup>3</sup>$  newton/metre<sup>2</sup> [N/m<sup>2</sup>]

8.5 Velocity [m/s] 1 m/s 196 .86 feet / minute fpm x  $5.0797x10^3$  metres/second [m/s] miles per hour [mph] 0 .447 metres/second  $\lceil m/s \rceil$ 

8.6 Capacity flow 1 litre/sec 0 .5886 x 10<sup>3</sup> ft<sup>3</sup>/min 1 m<sup>3</sup>/s 35 .3147 ft<sup>3</sup>/s [cusec]

- 8.7 Density Pound/inch<sup>3</sup> 27 .68 gram/centimeter 2.768 x 10<sup>4</sup> kilogram/ metre<sup>3</sup> [kg/m<sup>3</sup>] Ton/yard<sup>3</sup> 693.6 kilogram/metre<sup>3</sup> [kg/m<sup>3</sup>]
- 8 .8 Mass 1 pound [lb] 0 .45 kilogram [kg] 1 kilogram 2.20 pounds [lb] 1 stone 6 .35 kilogram [kg] 1 ounce [oz] 0 .03 kilogram [kg] 1 ton (short) 0.91 tonne (metric)
- 8.9 Energy BTU (British Thermal Unit) 1 055 Joule [J] 1 055 Newton-metre [Nm] 0 .252 kilocalorie 0 .02931x10<sup>3</sup> kilowatt-hour [kWh] 0 .393 x 10<sup>3</sup> horsepower-hour

#### General nomenclature and glossary

To ensure a proper understanding of coupling technology, it is important to be familiar with the terminology associated with the industry as a whole.

The following alphabetical listing, while basic in some areas, outlines the more commonly used terms and nomenclature. It is an ever-developing glossary under constant review and update. Refer also to Selection guidelines and evaluation tables.

A flexible coupling may be defined as:

"… a device, usually mechanical, that transmits power (torque) constantly, from one shaft to another, while allowing (if required), for some degree of misalignment (angular α°, parallel β, or a combination) and/or axial movement between the two shafts…"

AGMA (American Gear Manufacturers Association), the national authority in the US with respect to gear (and coupling) standards (e .g . minimum rating standards and coupling flange inter-connection) . (See also standards).

ANSI (American National Standards Institute), the governing body of all standards in the USA (See also standards).

Axial and axial direction: A projection or movement along the line of axis of rotation. For example, the position of a coupling hub on a shaft may be changed by sliding the hub in either direction, thus affecting its axial position on the shaft. An axial screw is used to secure a flange or hub to a machine member, whereby the screw is affixed parallel to the axis of rotation of the shaft.

Backlash: The amount of free play or movement between two rotating, mating parts . If one half of an elastomeric coupling is held rigid, and a torque applied to the other half, the amount of radial movement is referred to as backlash, and may be expressed in degrees, or 0.001 mm. (Backlash is not the same as stiffness (see above). Backlash is sometimes referred to as torsional rigidity.

In a torsionally rigid or backlash-free coupling, there will be zero play or movement between the driving and driven units . Each will rotate at exactly the same time, with no angular differential (°), usually measured in minutes or degrees .

Blade Pass Frequency (BPF) (→ fig. 1) A phenomenon that can be inherent in cooling tower (CT) fan drives with cardan shaft drives . It is where the passing of the blade over the shaft can set up a destructive resonance, especially if the cardan shaft DBSE's are large (in relation to shaft diameter) .

Bushing and taper bushing: A cylindrical sleeve used to adapt a bored part to a smaller diameter shaft. The taper bushing has a slightly tapered outside diameter, and is located in the hub element by means of a series of bolts or screws . Two main bushing methods are popular:

- Taper bushing
- QD (Quick Detachable referring to ease of installation) bushing dominant in the U.S. market, and usually only seen on imported machinery outside the Americas.

A more recent addition from Europe is the friction-locking/cone clamping element or locking assembly , which for SKF is series "FX" . Used extensively in servo-couplings for zero backlash, and positioning.

Bore: The central hole which is the mounting surface for the product or hub on the shaft. Close tolerances are required, typically referred to as transition or interference . 'Clearance' is normally only used for light duty applications.

Cardan shaft: A length of shaft, usually hollow in cross-section (for weight and strength benefits), mounted between two flanges of the respective couplings. For longer spans, a calculation is often necessary to check for whirling and buckling at critical speeds (frequencies).

The coupling may accept both angular and parallel offset combined . (For smaller span distances a spacer type insert is usually used.)

Damping: Usually referred to in relation to elastomeric couplings, (although the grid type coupling can also offer up to 30% damping) . This is the ability of the elastomeric material to dampen or change the frequency or resonance usually from the driver to the driven side . (**†** diagram 1)

Different elastomeric materials can be used to offer a range of characteristics in most coupling types . Damping can be critical if the drive system has similar common frequencies (Refer also to stiffness) .

Distance between shaft (Ends): The distance between the face of one shaft and that of the other. This is sometimes referred to in US publications as the BSE measurement (Between Shaft Ends, or more commonly, DBSE (Distance Between Shaft Ends)

Donut:The elastomeric element in a donut type elastomeric coupling (e .g . Centaflex)

Drop-out: The spacer type coupling is often referred to as a drop-out coupling. The drop-out portion fits between the two shaft ends, and is approximately equal to the DBSE dimension.

End-float: The ability of a coupling to move axially, usually to compensate for forces inherent in the system when at operating temperature.

Elastomer and elastomeric elements: Resilient materials through which the power of a coupling is transmitted . They are in some way attached to, or located at, the coupling halves, and usually made of rubber, synthetic rubber (NBR), or plastics-urethane, Hytrel, etc. Material selection is often dictated by environment.

Flange: A portion, usually of one coupling half, which extends outward from the normal outside diameter of the half, to a flange of similar size on the (driven) machine . As a rule, there is no hub with a bore on this coupling half, nor is there any shaft projecting from this portion of the (driven) machine.

Flexible couplings (and universal joints): Devices for transmitting mechanical power from one rotating shaft to another, while usually allowing for some degree of misalignment between the shafts.

Flexlink and disc pack: Metallic, flexible members of all steel couplings. They take the place of the elastomeric element. Power is transmitted through these metallic members, (alternately attached to the coupling hubs), and they allow for angular  $(\alpha)$ , and, in some cases, parallel ( $\varDelta_{1}$ ) misalignment.

Floating shaft: A configuration of a long shaft, mounted between two flexible couplings (usually single engagement). The arrangement allows the shaft to float between centres to find its best operating angle and position . The greater the distance between the two flex half hubs, the greater the allowable angular misalignment  $(\rightarrow$  fig. 2).

Keyway: The rectangular slot cut into the bore. Depending on the country, they may be to BS46, ISO or DIN 6885/1, or for shallow keyways, DIN 6885/3 . For the US market, typically to ASME B17.1

Dimensions vary between the US and other standards, with the European markets preferring rectangular keys, and the US favouring square keys . Either option is available however, for all markets (See also standards).

Note: Key tolerance fit (normal) should be N9, and P9 for close, tight fit.

kW (or Hp) / 100 r/min: This method of rating is shown in many US-based coupling catalogues, and allows easy estimation of the coupling power capacity. (Sometimes shown as Hp/c, 'c' being the Roman designation for 100. The rating is power, in kW or Hp, NOT torque.

 kW(Hp) x 100  $kW(Hp)/100$  r/min = r/min

To obtain the kW capacity of a coupling from the kW (Hp) / 100 r/min, multiply by the required r/min divided by 100 (e.g. at 1 440 r/min multiply by 14 .4… 960 r/min multiply by 9.60 etc.)

Length Thru' Bore (LTB): The effective length of the hole, or that portion of the length which is usable, and may be attached to the shaft.

Limits and Fits (See "Tolerances")

Misalignment – Angular  $[\alpha]$ : A measure of the angle between two shafts  $(\rightarrow$  fig. 3). It may be as an angular measurement (in degrees or minutes), or as a gap differential (X-Y) at two points 180° apart, and usually re-checked at 90° to the original .

Misalignment – Parallel [Δ]: The measure of the off-set between two shafts ( $\rightarrow$  fig. 4), and the summation of the difference  $(+/-)$ 

of both hubs to the centreline (axis of rotation).

Catalogue information usually shows the angular [α] and parallel [Δ] misalignment allowable for each coupling half, or the total permissible for the complete coupling. Check parameters!

In certain conditions there may a combination of both angular and parallel offset. Important: Not all coupling types are able to accommodate such a condition.

Outside diameter: The largest effective diameter of the product (e .g . flange, sleeve or cover diameter).

Overall length: The largest effective length of the product, part or fully assembled unit.

Overhung load (OHL, or  $F_{RA}$ ): The load or weight on a shaft as a result of the mounting of the coupling, pulley, sprocket, gear or other drive element on the shaft. Overhung load is expressed as the total of the load on the shaft. Allowable overhung loads usually refer to the load being applied at some point "X" (midway) along the shaft, or factored accordingly, if it is beyond the midway point from the last bearing.

$$
OHL = \frac{2 \times 9550 \times kW \times K_1}{r/min \times ped}
$$
[Newtons]

**Where** 



Power (Kilowatt – kW): The rate at which torque is applied . Since applied torque causes the shaft and its connections to rotate, a certain r/min results . The ISO measurement of power is the kilowatt [kW].

$$
kW = \frac{\text{Torque [Nm] } \times r/min}{9.550}
$$

Also

$$
kW = \frac{2 \times \pi \times r/min \times M_T}{60 \times 10^3}
$$

Note: Electrically, based on current [amp] readings, power may also be calculated by the following formulae. This will give the demand power if the amps value is based on the drawn amps of the running motor and not on nameplate values.

$$
kW_E = \frac{\sqrt{3} \times V \times I \times \cos \phi \times \mu \xi_0}{1000} [kW]
$$

**Where** 



To convert kW to horsepower [Hp], divide kW by 0.746.

Radial: Any projection / direction outwardly from the centre of the shaft, or cylindricalshaped object. The centre-line of the projection normally passes through the axial centre-line of the object . Examples are capscrew holes, and the arms of coupling spiders.

Reactionary force [FR]: The force exerted onto the shaft by the coupling, due to misalignment and / or run-out and axial float. The resultant force is applied perpendicular to the coupling.

$$
F_{RA}
$$
 or  $F_{RB} = 5600 \times \sqrt{\frac{P}{N}}$ 

**Where** 

 $F<sub>RA</sub>$  Load applied perpendicular to the coupling [N], at pos A1)

- P Power [kW]
- N Speed [r/min] at the point being considered (e.g. 'A' or 'B')

R/min: Revolutions per minute. In European catalogues, this is sometimes written as min<sup>-1</sup>, or just n<sub>1</sub>.

RSB (Rough Stock Bore): The minimum mandrel or pilot bore of the hub of the coupling.

#### Runout and eccentricity (T.I.R.)

A measure of the amount that a cylindrical body is off its true centre.

When a coupling half is rotated on the shaft, the outside diameter of the coupling

<sup>&</sup>lt;sup>1)</sup> A common method/nomenclature is to refer to the LS (low speed) shaft loadings in gear units as FRA, and on the input/high speed, or HS, as FRB.

may be slightly 'off to one side', axially and / or radially . A dial indicator, measuring in 0 .001 mm increments, is used to measure the run-out. This measurement reading is often referred to as the "T.I.R." – total indicator read-out, which measures the total 'play, as  $+/-$ .

Set screw: Headless screw, with hex headshaped socket, used over the keyway to keep the key in place and to prevent the product (hub) moving axially.

Shaft: Normally a cylindrical shaped machine member which rotates, and provides the means for supporting a coupling hub, U-joint, pulley, sprocket gear or other drive element. It may also be square or hexagonal in profile.

Sleeve: The elastomeric element of a shear type elastomeric coupling.

Slider coupling: Usually used in flanged gear couplings, the internal gear of the cover has an extended length (width) of the gear teeth cut into it. This allows the hub(s) to move axially for a set distance, while still maintaining full load (torque) capability. ( $\rightarrow$  fig. 5)

However the angular misalignment capability of the slider coupling is reduced by up to 50% of that of the equivalent standard configuration.

Available in three types of slider designs, and width (axial movement) options . They are available in both double (DE) or single (SE) engagement types .

Spacer: The portion of the flexible coupling (or U-joint) which spans the gap between the ends of the shaft. Spacer type couplings are used when the distance from one shaft end to another, is greater than the distance between normal coupling spacing.  $(\rightarrow$  fig. 6)

Special spacers may be used when the shaft spacing cannot be bridged by a standard coupling. There are international recommendations for the coupling length (API (US) and ISO/DIN) .

The metric lengths are 100 mm, 140 mm and 180 mm. The US standards are  $3\frac{1}{2}$ ", 5" and 7".

This type of coupling is extensively used in the pump industry, allowing pump maintenance without the need to remove or relocate the motor, and rapid repair in any instances of gland packs etc.

Spider: The elastomeric element of a flexible coupling, usually with 4 or 6 arms or fingers. They may be straight, curved or circular in shape . Typical materials are nitrile (NBR), neoprene, urethane (often available in various durometer °A hardnesses), and hytrel. In some types, a bronze insert is also available for slow speed extreme applications. (See also "L" Jaw).

Standards: Usually dimensional (and sometimes minimal performance) criteria set by a number of recognized organisations worldwide.

Common standards organisations and references include:

- AGMA American Gear Manufacturers Association (USA)
- ANSI American National Standards Institute (USA)
- ASME American Society of Mechanical Engineers (USA)
- BSI British Standards Institute (UK)
- DIN Deutsches Institut für Normung (Germany)
- IEC International Electrical Code (International – metric)



- ISO International Standards Organisation (International – metric)
- JIS Japanese Industrial Standard (Japan)
- NEMA National Electrical Manufacturers Association (USA)
- SAE Society of Mechanical Engineers (USA)
- SI Systeme Internationale (International – metric)

Stiffness: (also called torsional stiffness  $[\varphi_{\scriptscriptstyle{\overline{1}}}]$  is usually expressed in Nm/rad. A measure of the compression of the elastomeric element of the coupling, when torque is applied . It may be visualised as a twisting action, and is most obvious in couplings which transfer torque from one half to another through a rubber-like or plastic element such as a spider, donut or sleeve.

**Tightening torque**: [M<sub>D</sub>]: The torque required to properly seat a setscrew, capscrew or bolt in an assembly of any kind. Applied to the setscrew, for example, it is the force applied to the wrench multiplied by the length of the wrench . (See torque below).

The actual tightening torque is generally given in the coupling assembly and installation instructions . It is important to note that all technical/performance details and specifications pertaining to the coupling's performance, will be based on correctly tightened (torqued) bolts and setscrews, where applicable.



For most coupling bores, fits are typically transition (e.g. H7) or intereference (e.g. K7 or M7 depending on diameter) and depending on duty and application.

Clearance (e.g. F7) should only be used for lighter duty applications with uniform loads. (Refer to 'Keyway').

Bore tolerances should also be referenced to the shaft tolerance for good fit.

The ISO system of Limits and fits (metric) is covered by global and national standards, some of which are listed below, for reference:



Torque: (MT) The force (in Newtons) required to turn a shaft, multiplied by the radius (metres) at which the force is applied. The standard unit of torque in ISO terminology is Newton-metre [Nm].

Torque [M<sub>T</sub>] = F x r [Nm]

(It may also be derived by using the "Power" [kW] formulae shown on page 91.)







# Lubrication

Grease lubrication for gear and grid couplings

For longevity, the greases used in gear or grid couplings must have characteristics different from general purpose greases, due to the fact that the couplings are rotating. At higher speeds in particular, the centrifugal forces induced by these higher speeds may cause the grease components to separate, resulting in breakdown and subsequent inability to adequately protect metal – metal contact faces.

#### Typical specifications:

- High resistance to centrifugal forces and separation.
- Maintaining good lubricating properties
- Both stain and corrosion free
- Minimum base oil viscosity 600 mm<sup>2</sup>/sec at 40O °C





Table 2

<sup>1)</sup> Coupling speed range with NLGI 0 greases is from

zero to maximums shown.<br>For northern climate applications. For continuous op-<br>eration at constant ambient temperatures less than 0<br>°F or –18 °C (e.g. refrigeration systems), consult SKF.

Grease recommendations are generally based on typical ambient temperature ranges of –30O to 95O °C, (some are available up to 1 40O °C) and selection should be based on a 6-month lubrication cycle, depending on loading, temperature and ambient conditions such as dirt, contamination, overload conditions, alignment etc.

For normal duty, National Lubricating Grease Institute recommendation is for NLGI#1 (with EP) grade greases . At lower speeds, (typically below 300 r/min), a grease complying with NLGI #0 may be used. At very low speeds, the use of oil (with moderate EP capabilities) should be considered.

(Note: In such cases, the coupling should be totally sealed for oil use, including sealing of the keyways).

Following are some typical specifications for different greases operating in medium conditions, loads and speeds. Commonly used brands are listed, though not limited to those shown.

#### Table 3





# Related products

## Shaft alignment tools



#### TKSA 11

#### New technology makes shaft alignment easier and more affordable

The SKF TKSA 11 is an innovative shaft alignment tool that uses smartphones and tablets and intuitively guides the user through the shaft alignment process . With a focus on the core alignment tasks, the TKSA 11 is designed to be a very easy-touse instrument that is especially suitable for alignment learners and compact applications . The SKF TKSA 11 uses inductive proximity sensors, enabling accurate and reliable shaft alignment to be affordable for every budget.

## TKSA 51

#### Comprehensive and intuitive shaft alignment utilising tablets and smart phones

The TKSA 51 shaft alignment tool provides high measurement flexibility and performance suitable for entry-level to expert alignment jobs . Designed to work with the SKF shaft alignment apps on a tablet or smart phone, this intuitive tool is easy to use and requires no special training. The included accessories enable use of the TKSA 51 for a wide range of alignment applications with horizontal and vertical shafts, such as motors, drives, fans, pumps, gearboxes and more.

### TKSA 31

#### The intuitive and affordable laser shaft alignment system

The ergonomic display unit with touch screen makes the instrument very easy to use and the built-in machine library helps storing alignment reports for multiple machines. Large sized laser detectors in the measuring heads reduce the need for pre-alignments and the embedded soft foot tool helps establish the foundation for a successful alignment. Additional functions such as live view and automatic measurement support fast and effective alignment tasks.

## TKSA 71

#### Versatility and performance for professional alignment

Superior alignment performance and longterm industrial durability are achieved with an innovative instrument design that offers high measurement accuracy and excellent protection against dust and water in harsh environments . Designed for professional alignment in harsh industrial environments. The instrument is very versatile with ultracompact measuring units for use in extremely narrow spaces . Its dedicated software applications enable different types of alignments, including horizontal and vertical shafts, spacer shafts and machine trains.

### TKSA 41

#### The advanced laser shaft alignment system with enhanced measuring and reporting capabilities

The TKSA 41 is a laser alignment solution for achieving accurate shaft alignments . With two wireless measurement units, large sized detectors and powerful lasers, the instrument performs precise measurements in even the most challenging conditions . The ergonomic display unit with intuitive touch screen navigation makes your alignments fast and easy, whilst innovative features, like the "free measurement", increase the alignment performance.

### Alignement apps

Designed for use without prior training The TKSA 51 and 71 function quickly and intuitively using software apps tailored for different alignment jobs. These simple-touse apps are available free of charge for both Android and iOS platforms . Common features include comprehensive, automatic reports, export and sharing options, machine library with QR code identification, instructional videos within the app, built-in tolerance guidelines, 3-D live view, disturbance compensation and a fully functional demonstration mode.

## Selection chart







1) With supplied USB cables

## Machinery shims TMAS series

#### For accurate vertical machinery alignment

Accurate machine adjustment is an essential element of any alignment process.

- Made of high quality stainless steel, allowing re-use
- Easy to fit and to remove
- Close tolerances for accurate alignment
- Thickness clearly marked on each shim
- Fully de-burred
- Pre-cut shims are supplied in packs of 10 and complete kits are also available







Pack designation Thickness (mm)

0 .05 0 .10  $0.20$ 0 .25 0 .40 0 .50 0 .70 1 .00 2 .00 3 .00

TMAS 75-005 TMAS 75-010 TMAS 75-020 TMAS 75-025 TMAS 75-040 TMAS 75-050 TMAS 75-070 TMAS 75-100 TMAS 75-200 TMAS 75-300







Each pack designation consists of 10 shims .



Pack designation Thickness (mm)

A 125 mm B 125 mm C 45 mm

0 .05 0 .10  $0.20$ 0 .25 0 .40 0 .50 0.70 1 .00 2 .00 3 .00

TMAS 125-005 TMAS 125-010 TMAS 125-020 TMAS 125-025 TMAS 125-040 TMAS 125-050 TMAS 125-070 TMAS 125-100 TMAS 125-200 TMAS 125-300



## Stroboscopes TKRS series

#### High-performance, hand-held stroboscopes for visual inspection

SKF offers a wide range of portable TKRS stroboscopes for visual inspection of running machines in challenging industrial environments . These portable tools provide early detection of abnormalities to help schedule maintenance tasks and reduce additional loads on rotating equipment in order to reach planned performance levels . Designed for ease of use, the four TKRS models offer from 3 to 118 ultra-bright LEDs . Each stroboscope features a large screen and multifunctional selector switch to help you quickly navigate to the correct menu . Brightness and performance levels are adjustable.

#### TKRS 11

- Quick speed selection with rotary button
- Black and white LCD display
- Three ultra-bright LEDs

### TKRS 21

- High luminescence with seven ultra-bright LEDs
- Multi-line backlit TFT

## TKRS 31

- Built-in laser tachometer with flash synchronization
- Pro-mode with additional features like slow motion phase shift
- Trigger input and output with signal modification









### TKRS 41

- Extreme luminescence with 118 ultra-bright LEDs
- Portable operation with built-in rechargeable battery
- Continuous operation for long term inspection with power adapter
- Flash synchronization from laser tachometer or trigger input

#### Notes



#### skf.com | skf.com/powertransmission | skf.com/mapro

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 $\mathbb{R}^n$ 

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